

RUSSIAN MARITIME REGISTER OF SHIPPING

RULES

FOR THE CLASSIFICATION AND CONSTRUCTION OF SEA-GOING SHIPS

VOLUME

3



Saint-Petersburg
Edition 2012

Rules for the Classification and Construction of Sea-Going Ships of Russian Maritime Register of Shipping have been approved in accordance with the established approval procedure. The date of coming into force of the present Rules is 1 January 2012.

The Rules are based on the fourteenth edition (2011) taking into account amendments developed immediately before publication.

The unified requirements, interpretations and recommendations of the International Association of Classification Societies (IACS) and the relevant resolutions of the International Maritime Organization (IMO) have been taken into consideration in the Rules.

The Rules are published in five volumes.

General Regulations for the Classification and Other Activity, Part I "Classification", Part II "Hull", Part III "Equipment, Arrangements and Outfit", Part IV "Stability", Part V "Subdivision", Part VI "Fire Protection" are included in Volume 1.

Part VII "Machinery Installations", Part VIII "Systems and Piping", Part IX "Machinery", Part X "Boilers, Heat Exchangers and Pressure Vessels", Part XI "Electrical Equipment", Part XII "Refrigerating Plants", Part XIII "Materials", Part XIV "Welding", Part XV "Automation", Part XVI "Hull Structure and Strength of Glass-Reinforced Plastic Ships and Boats" are included in Volume 2.

Part XVII "Distinguishing Marks and Descriptive Notations in the Class Notation Specifying Structural and Operational Particulars of Ships" is included in Volume 3.

Part XVIII "Common Structural Rules for Double Hull Oil Tankers" (in electronic format only) is included in Volume 4.

In case of contradictions in the texts the English text shall be considered as the original.

Part XIX "Common Structural Rules for Bulk Carriers" (in electronic format only) is included in Volume 5.

In case of contradictions in the texts the English text shall be considered as the original.

The text of the Rules in the Russian language published in 2011 shall be considered as the original.

As compared to the previous edition (2011), the fifteenth edition contains the following amendments.

RULES FOR THE CLASSIFICATION AND CONSTRUCTION OF SEA-GOING SHIPS

PART XVII. DISTINGUISHING MARKS AND DESCRIPTIVE NOTATIONS IN THE CLASS NOTATION SPECIFYING STRUCTURAL AND OPERATIONAL PARTICULARS OF SHIPS

1. Section 1: Chapter 1.2 has been amended considering IACS UR I2.
2. Section 2: para 2.1.2.1: the definition of "Escort tug" has been specified;
a new para 2.3.2.1 specifying the procedure for full scale trials has been introduced.
3. Section 3: paras 3.5.2 and 3.6.2: the provisions of revised Annex VI to MAPIIOJI 73/78 adopted by IMO resolution MEPC.176(58) and revised NO_x Technical Code have been specified;
para 3.5.3.8: the provisions of the International Convention on the Control of Harmful Anti-Fouling Systems on Ships, 2001 have been specified;
the provisions of IMO resolutions MEPC.182(59), MEPC.184(59), MEPC.185(59) and MEPC.186(59) have been specified in other paras.
4. Section 7: para 7.6.1: the requirements for rated power and required rated torque at propeller shafts of ice class ships have been specified.
5. Editorial amendments have been made.

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1 REQUIREMENTS FOR POLAR CLASS SHIPS

1.1 POLAR CLASS DESCRIPTIONS AND APPLICATION

1.1.1 Application.

1.1.1.1 The requirements for polar class ships apply to ships constructed of steel and intended for navigation in ice-infested polar waters, except icebreakers (refer to 1.1.1.3).

The requirements of the present Section apply to ships contracted for construction on or after 1 March 2008.

Note. The date of "contract for construction" means the date on which the contract to build the ship is signed between the prospective owner and the shipbuilder. For further details regarding the date of "contract for construction" refer to 1.1.2, Part I "Classification".

1.1.1.2 Ships that comply with requirements of 1.2 and 1.3 can be considered for a polar class notation as listed in Table 1.1.1.2. The requirements of 1.2 and 1.3 are in addition to the Register requirements for ships without ice strengthening. If the hull and machinery are constructed such as to comply with the requirements of different polar classes, then both the hull and machinery shall be assigned the lower of these classes in the Classification Certificate. Compliance of the hull or machinery with the requirements of a higher polar class shall also be indicated in column "Other characteristics" of the Classification Certificate.

1.1.1.3 Ships that shall receive an "**Icebreaker**" notation may have additional requirements and shall receive special consideration. "**Icebreaker**" refers to any ship having an operational profile that includes escort or ice management functions, having powering and dimensions that allow it to undertake aggressive operations in ice-covered waters, and having a Classification Certificate endorsed with this notation.

1.1.2 Polar classes.

1.1.2.1 The polar class (PC) notations and descriptions are given in Table 1.1.1.2. It is the responsibility of the shipowner to select an appropriate polar class. The descriptions in Table 1.1.1.2 are intended to guide owners, designers and flag state administrations in selecting an appropriate polar class to match the requirements for the ship with its intended voyage or service.

1.1.2.2 The polar class notation is used throughout the present Section to convey the differences between classes with respect to operational capability and strength.

1.1.3 Upper and lower ice waterlines.

1.1.3.1 The upper and lower ice waterlines upon which the design of the ship has been based shall be indicated in the Classification Certificate. The upper ice waterline (UIWL) shall be defined by the maximum draughts fore, amidships and aft. The lower ice waterline (LIWL) shall be defined by the minimum draughts fore, amidships and aft.

1.1.3.2 The lower ice waterline shall be determined with due regard to the ship's ice-going capability in the ballast loading conditions (e.g. propeller submergence).

1.2 STRUCTURAL REQUIREMENTS FOR POLAR CLASS SHIPS

1.2.1 Application.

1.2.1.1 The requirements of the present Section shall be applied to polar class ships indicated in 1.1.

1.2.2 Hull areas.

1.2.2.1 The hull of all polar class ships is divided into areas reflecting the magnitude of the loads that are expected to act upon them. In the longitudinal direction, there are four regions: bow (B), bow intermediate (BI), midbody (M) and stern (S). The bow intermediate, midbody and stern regions are further divided in the vertical direction into the bottom (b), lower (l) and ice belt (i) regions. The extent of each hull area is illustrated in Fig. 1.2.2.1.

1.2.2.2 The upper ice waterline (UIWL) and lower ice waterline (LIWL) are as defined in 1.1.3.

1.2.2.3 Fig. 1.2.2.1 notwithstanding, at no time shall the boundary between the bow and bow intermediate regions be forward of the intersection point of the line of the stem and the ship baseline.

1.2.2.4 Fig. 1.2.2.1 notwithstanding, the aft boundary of the bow region need not be more than 0,45L aft of the forward perpendicular (FP).

1.2.2.5 The boundary between the bottom and lower regions shall be taken at the point where the shell is inclined 7° from horizontal.

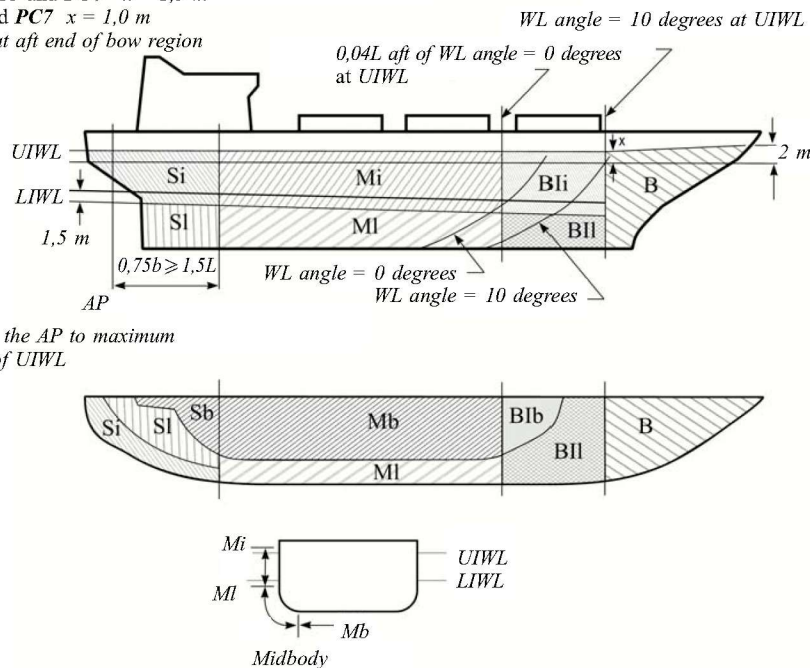
Table 1.1.1.2

Polar class descriptions	
Polar class	Ice description (based on WMO Sea Ice Nomenclature)
PC1	Year-round operation in all polar waters
PC2	Year-round operation in moderate multi-year ice conditions
PC3	Year-round operation in second-year ice which may include multi-year ice inclusions
PC4	Year-round operation in thick first-year ice which may include old ice inclusions
PC5	Year-round operation in medium first-year ice which may include old ice inclusions
PC6	Summer/autumn operation in medium first-year ice which may include old ice inclusions
PC7	Summer/autumn operation in thin first-year ice which may include old ice inclusions

For **PC1, PC2, PC3** and **PC4** $x = 1,5 \text{ m}$

For **PC5, PC6** and **PC7** $x = 1,0 \text{ m}$

with x measured at aft end of bow region



b = distance from the AP to maximum half breadth of UIWL

Fig. 1.2.2.1
Hull area extents

1.2.2.6 If a ship is intended to operate astern in ice regions, the aft section of the ship shall be designed using the bow and bow intermediate hull area requirements.

1.2.3 Design ice loads.

1.2.3.1 General.

1.2.3.1.1 For ships of all polar classes, a glancing impact on the bow is the design scenario for determining the scantlings required to resist ice loads.

1.2.3.1.2 The design ice load is characterized by an average pressure P_{avg} uniformly distributed over a rectangular load patch of height b and width w .

1.2.3.1.3 Within the bow area of all polar classes, and within the bow intermediate ice belt area of polar classes **PC6** and **PC7**, the ice load parameters are functions of the actual bow shape. To determine the ice load parameters P_{avg} , b and w , it is required to calculate the following ice load characteristics for sub-regions of the bow area; shape coefficient f_{a_i} , total glancing impact force F_i , line load Q_i and pressure P_i .

1.2.3.1.4 In other ice-strengthened areas, the ice load parameters P_{avg} , b_{NonBow} and w_{NonBow} are determined independently of the hull shape and based on a fixed load patch aspect ratio, $AR = 3,6$.

1.2.3.1.5 Design ice forces calculated according to 1.2.3.2 are only valid for ships with icebreaking forms. Design ice forces for any other bow forms shall be specially considered by the Register.

1.2.3.1.6 Ship structures that are not directly subjected to ice loads may still experience inertial loads of stowed cargo and equipment resulting from ship/ice interaction. These inertial loads, based on accelerations determined according to the procedure approved by the Register, shall be considered in the design of these structures.

1.2.3.2 Glancing impact load characteristics.

1.2.3.2.1 The parameters defining the glancing impact load characteristics are reflected in the class factors listed in Table 1.2.3.2.1.

Table 1.2.3.2.1

Class factors

Polar class	Crushing failure class factor CF_C	Flexural failure class factor CF_F	Load patch dimensions class factor CF_D	Displacement class factor CF_{DIS}	Longitudinal strength class factor CF_L
PC1	17,69	68,60	2,01	250	7,46
PC2	9,89	46,80	1,75	210	5,46
PC3	6,06	21,17	1,53	180	4,17
PC4	4,50	13,48	1,42	130	3,15
PC5	3,10	9,00	1,31	70	2,50
PC6	2,40	5,49	1,17	40	2,37
PC7	1,80	4,06	1,11	22	1,81

1.2.3.2.1.1 Bow area.

1.2.3.2.1.1.1 In the bow area, the force F , line load Q , pressure P and load patch aspect ratio AR associated with the glancing impact load scenario are functions of the hull angles measured at the upper ice waterline. The influence of the hull angles is captured through calculation of a bow shape coefficient fa . The hull angles are defined in Fig. 1.2.3.2.1.1.1.

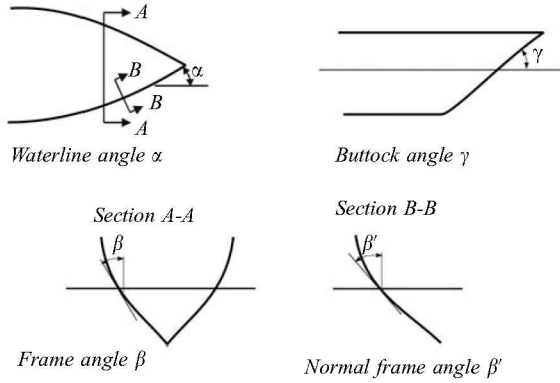


Fig. 1.2.3.2.1.1.1

Definition of hull angles

Notes: β' = normal frame angle at upper ice waterline, deg.;
 α = upper ice waterline angle, deg.;
 γ = buttock angle at upper ice waterline (angle of buttock line measured from horizontal), deg.;
 $\text{tg}\beta = \text{tg}\alpha/\text{tg}\gamma$;
 $\text{tg}\beta' = \text{tg}\beta/\cos\alpha$.

1.2.3.2.1.1.2 The waterline length of the bow region shall generally be divided into 4 sub-regions of equal length. The force F , line load Q , pressure P and load patch aspect ratio AR shall be calculated with respect to the mid-length position of each sub-region (each maximum of F , Q and P shall be used in the calculation of the ice load parameters P_{avg} , b and w).

1.2.3.2.1.1.3 The bow area load characteristics are determined as follows:

.1 shape coefficient fa_i shall be taken as:

$$fa_i = \min(fa_{i,1}; fa_{i,2}; fa_{i,3}) \quad (1.2.3.2.1.1.3.1-1)$$

where

$$fa_{i,1} = (0,097 - 0,68(x/L - 0,15)^2) \cdot \alpha_i/(\beta_i')^{0,5}; \quad (1.2.3.2.1.1.3.1-2)$$

$$fa_{i,2} = 1,2CF_F/(\sin(\beta_i') \cdot CF_C \cdot D^{0,64}); \quad (1.2.3.2.1.1.3.1-3)$$

$$fa_{i,3} = 0,60; \quad (1.2.3.2.1.1.3.1-4)$$

i = sub-region considered;
 L = ship length as defined in 1.1.3, Part II "Hull", but measured on the upper ice waterline (UIWL), in m;
 x = distance from the forward perpendicular to station under consideration, m;
 α = waterline angle, deg. (refer to Fig. 1.2.3.2.1.1.1);
 β' = normal frame angle, deg. (refer to Fig. 1.2.3.2.1.1.1);
 D = ship displacement, kt, not to be taken less than 5 kt;
 CF_C = refer to Table 1.2.3.2.1;
 CF_F = refer to Table 1.2.3.2.1;

.2 force F , MN:

$$F_i = fa_i \cdot CF_C \cdot D^{0,64} \quad (1.2.3.2.1.1.3.2)$$

where i = sub-region considered;

fa_i = shape coefficient of sub-region i ;

CF_C = refer to Table 1.2.3.2.1;

D = ship displacement, kt, not to be taken less than 5 kt;

.3 load patch aspect ratio AR :

$$AR_i = 7,46 \cdot \sin(\beta_i') \geq 1,3 \quad (1.2.3.2.1.1.3.3)$$

where i = sub-region considered;

β_i' = normal frame angle of sub-region i , deg.;

.4 line load Q , MN/m:

$$Q_i = F_i^{0,61} CF_D / AR_i^{0,35} \quad (1.2.3.2.1.1.3.4)$$

where i = sub-region considered;

F_i = force of sub-region i , MN;

CF_D = refer to Table 1.2.3.2.1;

AR_i = load patch aspect ratio of sub-region i ;

.5 pressure P , MPa:

$$P_i = F_i^{0,22} CF_D^2 AR_i^{0,3} \quad (1.2.3.2.1.1.3.5)$$

where i = sub-region considered;

F_i = force of sub-region i , MN;

CF_D = refer to Table 1.2.3.2.1;

AR_i = load patch aspect ratio of sub-region i .

1.2.3.2.2 Hull areas other than the bow.

1.2.3.2.2.1 In the hull areas other than the bow, the force F_{NonBow} and line load Q_{NonBow} used in the determination of the load patch dimensions b_{NonBow} , w_{NonBow} and design pressure P_{avg} are determined as follows:

.1 force F_{NonBow} , MN:

$$F_{NonBow} = 0,36CF_C DF \quad (1.2.3.2.2.1.1)$$

where CF_C = refer to Table 1.2.3.2.1;

DF = ship displacement factor:

$DF = D^{0,64}$ при $D \leq CF_{DIS}$;

$DF = CF_{DIS}^{0,64} + 0,10(D - CF_{DIS})$ при $D > CF_{DIS}$;

D = ship displacement, kt, not to be taken less than 10 kt;

CF_{DIS} = refer to Table 1.2.3.2.1;

.2 line load Q_{NonBow} , MN/m:

$$Q_{NonBow} = 0,639F_{NonBow}^{0,61} CF_D \quad (1.2.3.2.2.1.2)$$

where F_{NonBow} force from Formula (1.2.3.2.2.1.1), MN;

CF_D = refer to Table 1.2.3.2.1.

1.2.3.3 Design load patch.

1.2.3.3.1 In the bow area and the bow intermediate ice belt area for ships with class notation PC6 and PC7, the design load patch has dimensions of width w_{Bow} and height b_{Bow} , m, determined as follows:

$$w_{Bow} = F_{Bow}/Q_{Bow}; \quad (1.2.3.3.1-1)$$

$$b_{Bow} = Q_{Bow}/P_{Bow} \quad (1.2.3.3.1-2)$$

where F_{Bow} = maximum force F_i in the bow area (refer to 1.2.3.2.1.1.3.2), in MN;

Q_{Bow} = maximum line load Q_i in the bow area (refer to 1.2.3.2.1.1.3.4), in MN/m;

P_{Bow} = maximum pressure P_i in the bow area (refer to 1.2.3.2.1.1.3.5), in MPa.

1.2.3.3.2 In hull areas other than those covered by 1.2.3.3.1, the design load patch has dimensions of: width w_{NonBow} and height b_{NonBow} , m, determined as follows:

$$w_{NonBow} = F_{NonBow}/Q_{NonBow}; \quad (1.2.3.3.2-1)$$

$$b_{NonBow} = w_{NonBow}/3,6 \quad (1.2.3.3.2-2)$$

where F_{NonBow} = force determined by Formula (1.2.3.2.2.1.1), MN;
 Q_{NonBow} = line load determined by Formula (1.2.3.2.2.1.2) MN/m.

1.2.3.4 Pressure within the design load patch.

1.2.3.4.1 The average pressure P_{avg} , MPa, within a design load patch is determined as follows:

$$P_{avg} = F/(b \cdot w) \quad (1.2.3.4.1)$$

where $F = F_{Bow}$ or F_{NonBow} as appropriate for the hull area under consideration, MN;

$b = b_{Bow}$ or b_{NonBow} as appropriate for the hull area under consideration, m;

$w = w_{Bow}$ or w_{NonBow} as appropriate for the hull area under consideration, m.

1.2.3.4.2 Areas of higher, concentrated pressure exist within the load patch. In general, smaller areas have higher local pressures. Accordingly, the peak pressure factors listed in Table 1.2.3.4.2 are used to account for the pressure concentration on localized structural members.

1.2.3.5 Hull area factors.

1.2.3.5.1 Associated with each hull area is an area factor that reflects the relative magnitude of the load expected in that area. The area factor for each hull area is listed in Table 1.2.3.5.1.

1.2.3.5.2 In the event that a structural member spans across the boundary of a hull area, the largest hull area factor shall be used in the scantling determination of the member.

1.2.3.5.3 Due to their increased manoeuvrability, ships having propulsion arrangements with azimuthing thruster(s) or "podded" propellers shall have specially considered by the Register stern ice belt S_i and stern lower S_l hull area factors.

Table 1.2.3.4.2

Peak pressure factors

Structural member		Peak pressure factor PPF_i
Plating	Transversely-framed	$PPF_p = (1,8 - s) \geq 1,2$
	Longitudinally-framed	$PPF_p = (2,2 - 1,2 s) \geq 1,5$
Frames in transverse	With load distributing stringers	$PPF_t = (1,6 - s) \geq 1,0$
	Framing systems with no load distributing stringers	$PPF_t = (1,8 - s) \geq 1,2$
Load carrying stringers Side and bottom longitudinals Web frames		$PPF_s = 1, \quad \text{if } S_w \geq 0,5w$ $PPF_s = 2,0 - 2,0 \cdot S_w/w, \text{ if } S_w < 0,5w$
<p>where s = frame or longitudinal spacing, m; S_w = web frame spacing, m; w = ice load patch width, m.</p>		

Table 1.2.3.5.1

Hull area factors A_F

Hull area		Area	Polar class						
			PC1	PC2	PC3	PC4	PC5	PC6	PC7
Bow (<i>B</i>)	All	<i>B</i>	1,00	1,00	1,00	1,00	1,00	1,00	1,00
Bow Intermediate (<i>BI</i>)	Ice belt	<i>BI_i</i>	0,90	0,85	0,85	0,80	0,80	1,00*	1,00*
	Lower	<i>BI_l</i>	0,70	0,65	0,65	0,60	0,55	0,55	0,50
	Bottom	<i>BI_b</i>	0,55	0,50	0,45	0,40	0,35	0,30	0,25
Midbody (<i>M</i>)	Ice belt	<i>M_i</i>	0,70	0,65	0,55	0,55	0,50	0,45	0,45
	Lower	<i>M_l</i>	0,50	0,45	0,40	0,35	0,30	0,25	0,25
	Bottom	<i>M_b</i>	0,30	0,30	0,25	**	**	**	**
Stern (<i>S</i>)	Ice belt	<i>S_i</i>	0,75	0,70	0,65	0,60	0,50	0,40	0,35
	Lower	<i>S_l</i>	0,45	0,40	0,35	0,30	0,25	0,25	0,25
	Bottom	<i>S_b</i>	0,35	0,30	0,30	0,25	0,15	**	**

* Refer to 1.2.3.1.3.
 ** Indicates that strengthening for ice loads is not necessary.

1.2.4 Shell plate requirements.

1.2.4.1 The required minimum shell plate thickness t , mm, is determined by the formula

$$t = t_{net} + t_s \quad (1.2.4.1)$$

where t_{net} = plate thickness required to resist ice loads according to 1.2.4.2, mm;
 t_s = corrosion and abrasion allowance according to 1.2.11, mm.

1.2.4.2 The thickness of shell plating required to resist the design ice load t_{net} , mm, depends on the orientation of the framing.

In the case of transversely-framed plating ($\Omega \geq 70$ deg.), including all bottom plating, i.e. plating in hull areas BI_b , M_b and S_b , the net thickness is determined by the formula

$$t_{net} = 500s((AF \cdot PPF_p \cdot P_{avg})/\sigma_y)^{0.5}/(1 + s/2b) \quad (1.2.4.2-1)$$

where Ω = smallest angle between the chord of the waterline and the line of the first level framing as illustrated in Fig. 1.2.4.2, deg.;
 s = transverse frame spacing in transversely-framed ships or longitudinal frame spacing in longitudinally-framed ships, m;

AF = hull area factor from Table 1.2.3.5.1;

PPF_p = peak pressure factor from Table 1.2.3.4.2;

P_{avg} = average patch pressure according to Formula (1.2.3.4.1), MPa;

σ_y = minimum upper yield stress of the material, N/mm²;

b = height of design load patch, m, where $b \geq (l-s/4)$ in the case determined by Formula (1.2.4.2-1);

l = distance between frame supports, i.e. equal to the frame span as given in 1.2.5.5, but not reduced for any fitted end brackets, m. When a load-distributing stringer is fitted, the length l need not be taken larger than the distance from the stringer to the most distant frame support.

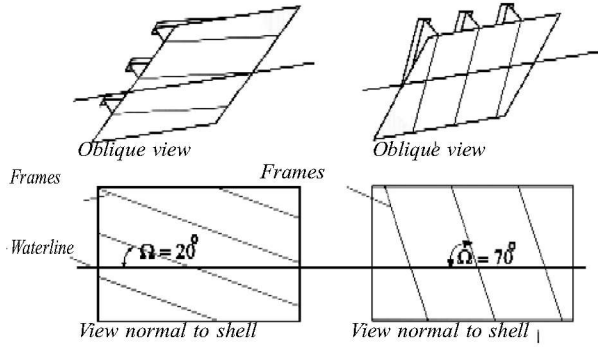


Fig. 1.2.4.2
Shell framing angle Ω

In the case of longitudinally-framed plating ($\Omega \leq 20$ deg.), when $b \geq s$, the net thickness is determined by the formula

$$t_{net} = 500s((AF \cdot PPF_p \cdot P_{avg})/\sigma_y)^{0.5}/(1 + s/2l) \quad (1.2.4.2-2)$$

In the case of longitudinally-framed plating ($\Omega \leq 20$ deg.), when $b < s$, the net thickness is determined by the formula

$$t_{net} = 500s((AF \cdot PPF_p \cdot P_{avg})/\sigma_y)^{0.5} \cdot (2b/s - (b/s)^2)^{0.5}/(1 + s/2l) \quad (1.2.4.2-3)$$

In the case of obliquely-framed plating ($70 \text{ deg} > \Omega > 20 \text{ deg}$), linear interpolation shall be used.

1.2.5 Framing. General.

1.2.5.1 Framing members of polar class ships shall be designed to withstand the ice loads defined in 1.2.3.

1.2.5.2 The term "framing member" refers to transverse and longitudinal local frames, load-carrying stringers and web frames in the areas of the hull exposed to ice pressure (refer to Fig. 1.2.2.1). Where load-distributing stringers have been fitted, the arrangement and scantlings of these shall be in accordance with the Register requirements.

1.2.5.3 The strength of a framing member is dependent upon the fixity that is provided at its supports. Fixity can be assumed where framing members are either continuous through the support or attached to a supporting section with a connection bracket. In other cases, simple support shall be assumed unless the connection can be demonstrated to provide significant rotational restraint. Fixity shall be ensured at the support of any framing which terminates within an ice-strengthened area.

1.2.5.4 The details of framing member intersection with other framing members, including plated structures, as well as the details for securing the ends of framing members at supporting sections, shall be in accordance with the requirements of the Register.

1.2.5.5 The design span of a framing member shall be determined on the basis of its moulded length. If brackets are fitted, the design span may be reduced in accordance with the Register requirements. Brackets shall be configured to ensure stability in the elastic and post-yield response regions.

1.2.5.6 When calculating the section modulus and shear area of a framing member, net thicknesses of the web, flange (if fitted) and attached shell plating shall be used. The shear area of a framing member may include that material contained over the full depth of the member, i.e. web area including portion of flange (if fitted) but excluding attached shell plating.

1.2.5.7 The actual net effective shear area A_w , cm², of a framing member is determined by the formula

$$A_w = ht_{wn} \sin \phi_w / 100 \quad (1.2.5.7)$$

where h = height of stiffener, mm, refer to Fig. 1.2.5.7;

t_{wn} = net web thickness, mm;

$t_{wn} = t_w - t_c$;

t_w = as built web thickness, mm (refer to Fig. 1.2.5.7);

t_c = corrosion deduction, mm, to be subtracted from the web and flange thickness (according to 3.10.4.1, Part II "Hull", but not less than t_s as required by 1.2.11.3);

ϕ_w = smallest angle between shell plate and stiffener web, measured at the midspan of the stiffener (refer to Fig. 1.2.5.7). The angle ϕ_w may be taken as 90 deg., provided the smallest angle is not less than 75 deg.

1.2.5.8 When the cross-sectional area of the attached plate flange exceeds the cross-sectional area of the local frame, the actual net effective plastic section modulus, Z_p , cm³, is determined by the formula

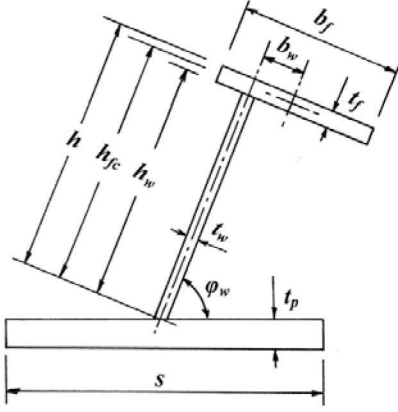


Fig. 1.2.5.7
Stiffener geometry

$$Z_p = A_{pn}t_{pn}/20 + \frac{h_w^2 t_{wn} \sin \varphi_w}{2000} + A_{fn}(h_{fc} \sin \varphi_w - b_w \cos \varphi_w)/10 \quad (1.2.5.8-1)$$

where h , t_{wn} , t_{cs} and φ_w are as given in 1.2.5.7 and s as given in 1.2.4.2;
 A_{pn} = net cross-sectional area of attached plate, cm^2 (equal to $10t_{pn}s$, but not to be taken greater than the net cross-sectional area of the local frame);
 t_{pn} = fitted net shell plate thickness, mm (shall comply with t_{net} as required by 1.2.4.2);
 h_w = height of local frame web, mm (refer to Fig. 1.2.5.7);
 A_{fn} = net cross-sectional area of local frame flange, cm^2 ;
 h_{fc} = height of local frame measured to centre of the flange area, mm, refer to Fig. 1.2.5.7;
 b_w = distance from mid thickness plane of local frame web to the centre of the flange area, mm (refer to Fig. 1.2.5.7).

When the cross-sectional area of the local frame exceeds the cross-sectional area of the attached plate flange, the plastic neutral axis is located at a distance z_{na} , mm, above the attached shell plate, determined by the formula

$$z_{na} = (100A_{fn} + ht_{wn} - 1000t_{pn}s)/2t_{wn} \quad (1.2.5.8-2)$$

and the net effective plastic section modulus Z_p , cm^3 , is determined by the formula

$$Z_p = t_{pn}s(z_{na} + t_{pn}/2) \sin \varphi_w + \left(\frac{((h_w - z_{na})^2 + z_{na}^2)t_{wn} \sin \varphi_w}{2000} + A_{fn}((h_{fc} - z_{na}) \sin \varphi_w - b_w \cos \varphi_w)/10 \right) \quad (1.2.5.8-3)$$

1.2.5.9 In the case of oblique framing arrangement ($70 \text{ deg.} > \Omega > 20 \text{ deg.}$, where Ω is defined as given in 1.2.4.2), linear interpolation shall be used.

1.2.6 Framing. Transversely-framed side structures and bottom structures.

1.2.6.1 The local frames in transversely-framed side structures and in bottom structures (i.e. hull areas BI_b , M_b and S_b) shall be dimensioned such that the combined effects of shear and bending do not exceed the plastic strength of the member. The plastic strength is defined by the magnitude of midspan load that causes the development of a plastic collapse mechanism.

1.2.6.2 The actual net effective shear area of the frame A_w , cm^2 , as defined in 1.2.5.7, shall comply with the following condition: $A_w \geq A_t$, where

$$A_t = 100^2 \cdot 0,5LL \cdot s(AF \cdot PPF_t \cdot P_{avg})/(0,577\sigma_y) \quad (1.2.6.2)$$

where LL = length of loaded portion of span = lesser of a and b , m;
 a = frame span as defined in 1.2.5.5, m;
 b = height of design ice load patch according to (1.2.3.3.1-2) or (1.2.3.3.2-2), m;
 s = transverse frame spacing, m;
 AF = refer to Table 1.2.3.5.1;
 PPF_t = refer to Table 1.2.3.4.2;
 P_{avg} = average pressure within load patch according to (1.2.3.4.1), MPa;
 σ_y = minimum upper yield stress of the material, N/mm^2 .

1.2.6.3 The actual net effective plastic section modulus of the plate/stiffener combination Z_p as defined in 1.2.5.8, shall comply with the following condition: $Z_p \geq Z_{pt}$, where Z_{pt} , cm^3 , shall be the greater calculated on the basis of two load conditions: ice load acting at the midspan of the transverse frame; and the ice load acting near a support.

$$Z_{pt} = 100^3 LL \cdot Y \cdot s(AF \cdot PPF_t \cdot P_{avg})a \cdot A_1/(4\sigma_y) \quad (1.2.6.3)$$

where AF , PPF_t , P_{avg} , LL , b , s , a and σ_y are as given in 1.2.6.2;

$$Y = 1 - 0,5(LL/a);$$

A_1 = maximum of:

$$A_{1A} = 1/(1 + j/2 + k_w j/2[(1 - a_1^2)^{0,5} - 1]);$$

$$A_{1B} = (1 - 1/(2a_1 \cdot Y))/(0,275 + 1,44k_z^{0,7});$$

j = 1 for framing with one simple support outside the ice-strengthened areas;

j = 2 for framing without any simple supports;

$$a_1 = A_t/A_w;$$

A_t = minimum shear area of transverse frame as given in 1.2.6.2, cm^2 ;

A_w = effective net shear area of transverse frame (calculated according to 1.2.5.7), cm^2 ;

$$k_w = 1/(1 + 2A_{fn}/A_w), \text{ with } A_{fn} \text{ as given in 1.2.5.8;}$$

$$k_z = z_p/Z_p, \text{ in general;}$$

$k_z = 0,0$, when the frame is arranged with end bracket;

z_p = sum of individual plastic section moduli of flange and shell plate as fitted, cm^3 ;

$$z_p = (b_f t_{fn}^2/4 + b_{eff} t_{pn}^2/4)/1000;$$

b_f = flange breadth, mm, refer to Fig. 1.2.5.7;

t_{fn} = net flange thickness, mm;

$t_{fn} = t_f - t_c$ as given in 1.2.5.7;

t_f = as-built flange thickness, mm, refer to Fig. 1.2.5.7;

t_{pn} = the fitted net shell plate thickness, mm (not to be less than t_{net} as given in 1.2.4);

b_{eff} = effective width of shell plate flange, mm;

$$b_{eff} = 500s;$$

Z_p = net effective plastic section modulus of transverse frame (calculated according to 1.2.5.8), cm^3 .

1.2.6.4 The scantlings of the frame shall meet the structural stability requirements of 1.2.9.

1.2.7 Framing. Side longitudinals (longitudinally-framed ships).

1.2.7.1 Side longitudinals shall be dimensioned such that the combined effects of shear and bending do not exceed the plastic strength of the member. The plastic strength is defined by the magnitude of midspan load that causes the development of a plastic collapse mechanism.

1.2.7.2 The actual net effective shear area of the frame A_w as defined in 1.2.5.7, shall comply with the following condition: $A_w \geq A_L$, where

$$A_L = 100^2 (AF \cdot PPF_s \cdot P_{avg}) \cdot 0,5b_1a / (0,577\sigma_y), \text{ cm}^2 \quad (1.2.7.2)$$

where AF = refer to Table 1.2.3.5.1;

PPF_s = refer to Table 1.2.3.4.2;

P_{avg} = average pressure within load patch according to (1.2.3.4.1), MPa;

$b_1 = k_0 b_2$, m;

$k_0 = 1 - 0,3/b'$;

$b' = b/s$;

b = height of design ice load patch from (1.2.3.3.1-2) or (1.2.3.3.2-2), m;

s = spacing of longitudinal frames, m;

$b_2 = b(1 - 0,25b')$, m, if $b' < 2$;

$b_2 = s$, m, if $b' \geq 2$;

a = longitudinal design span as given in 1.2.5.5, m;

σ_y = minimum upper yield stress of the material, N/mm².

1.2.7.3 The actual net effective plastic section modulus of the plate/stiffener combination Z_p as defined in 1.2.5.8, shall comply with the following condition: $Z_p \geq Z_{pL}$, where

$$Z_{pL} = 100^3 (AF \cdot PPF_s \cdot P_{avg}) b_1 a^2 A_4 / 8\sigma_y, \text{ cm}^3 \quad (1.2.7.3)$$

where AF , PPF_s , P_{avg} , b_1 , a and σ_y are as given in 1.2.7.2;

$A_4 = 1/(2 + k_{wl}[(1 - a_4)^{0,5} - 1])$;

$a_4 = A_L/A_w$;

A_L = minimum shear area for longitudinal as given in 1.2.7.2, cm²;

A_w = net effective shear area of longitudinal (calculated according to 1.2.5.7), cm²;

$k_{wl} = 1/(1 + 2A_{fn}/A_w)$ with A_{fn} as given in 1.2.5.8.

1.2.7.4 The scantlings of the longitudinals shall meet the structural stability requirements of 1.2.9.

1.2.8 Framing. Web frame and load-carrying stringers.

1.2.8.1 Web frames and load-carrying stringers shall be designed to withstand the ice load patch as defined in 1.2.3. The load patch shall be applied at locations where the capacity of these members under the combined effects of bending and shear is minimised.

1.2.8.2 Web frames and load-carrying stringers shall be dimensioned such that the combined effects of shear and bending do not exceed the limit state(s) defined by the Register. Where these members form part of a structural grillage system, appropriate methods of analysis shall be used. Where the structural configuration is such that members do not form part of a grillage system, the appropriate peak pressure factor PPF from Table 1.2.3.4.2 shall be used. Special attention shall be paid to the shear capacity in way of lightening holes and cutouts in way of intersecting members.

1.2.8.3 The scantlings of web frames and load-carrying stringers shall meet the structural stability requirements of 1.2.9.

1.2.9 Framing. Structural stability.

1.2.9.1 To prevent local buckling in the web, the ratio of web height h_w to net web thickness t_{wn} of any framing member shall not exceed:

for flat bar sections:

$$h_w / t_{wn} \leq 282 / \sigma_y^{0,5}; \quad (1.2.9.1-1)$$

for bulb, tee and angle sections:

$$h_w / t_{wn} \leq 805 / \sigma_y^{0,5} \quad (1.2.9.1-2)$$

where h_w = web height;

t_{wn} = net web thickness;

σ_y = minimum upper yield stress of the material, N/mm².

1.2.9.2 Framing members for which it is not practicable to meet the requirements of 1.2.9.1 (e.g. load carrying stringers or deep web frames) are required to have their webs effectively stiffened. The scantlings of the web stiffeners shall ensure the structural stability of the framing member. The minimum net web thickness for these framing members t_{wn} , mm, is determined by the formula

$$t_{wn} = 2,63 \cdot 10^{-3} c_1 \sqrt{\frac{\sigma_y}{5,34 + 4(c_1/c_2)^2}} \quad (1.2.9.2)$$

where $c_1 = h_w - 0,8h$, mm;

h_w = web height of stringer/web frame, mm (refer to Fig. 1.2.9.2);

h = height of framing member penetrating the member under consideration (0 if no such framing member), mm (refer to Fig. 1.2.9.2);

c_2 = spacing between supporting structure oriented perpendicular to the member under consideration, mm (refer to Fig. 1.2.9.2);

σ_y = minimum upper yield stress of the material, N/mm².

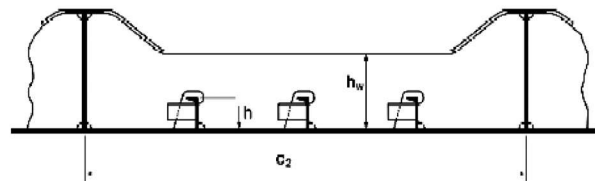


Fig. 1.2.9.2
Parameter definition for web stiffening

1.2.9.3 In addition, the following shall be satisfied:

$$t_{wn} \geq 0,35 t_{pn} (\sigma_y / 235)^{0,5} \quad (1.2.9.3)$$

where σ_y = minimum upper yield stress of the material, N/mm²;

t_{wn} = net thickness of the web, mm;

t_{pn} = net thickness of the shell plate in way the framing member, mm.

1.2.9.4 To prevent local flange buckling of welded profiles, the following shall be satisfied:

1 the flange width b_f , mm, shall not be less than five times the net thickness of the web t_{wn} ;

2 the flange outstand b_{out} , mm, shall meet the following requirement:

$$b_{out} / t_{fn} \leq 155 / \sigma_y^{0,5} \quad (1.2.9.4.2)$$

where t_{fn} = net thickness of flange, mm;

σ_y = minimum upper yield stress of the material, N/mm².

1.2.10 Plated structures.

1.2.10.1 Plated structures are those stiffened plate elements in contact with the hull and subject to ice loads. These requirements are applicable to an inboard extent which is the lesser of:

- .1 web height of adjacent parallel web frame or stringer; or
- .2 2,5 times the depth of framing that intersects the plated structure.

1.2.10.2 The thickness of the plating and the scantlings of attached stiffeners shall be such that the degree of end fixity necessary for the shell framing is ensured.

1.2.10.3 The stability of the plated structure shall adequately withstand the ice loads defined in 1.2.3.

1.2.11 Corrosion/abrasion additions and steel renewal.

1.2.11.1 Effective protection against corrosion and ice-induced abrasion is recommended for all external surfaces of the shell plating for all polar ships.

1.2.11.2 The values of corrosion/abrasion additions t_s to be used in determining the shell plate thickness for each polar class are listed in Table 1.2.11.2.

Table 1.2.11.2

Corrosion/abrasion additions for shell plating

Hull area	t_s , mm					
	With effective protection			Without effective protection		
	PC1 to PC3	PC4 and PC5	PC6 and PC7	PC1 to PC3	PC4 and PC5	PC6 and PC7
B, BI _i	3,5	2,5	2,0	7,0	5,0	4,0
BI _b , M _i , S _i	2,5	2,0	2,0	5,0	4,0	3,0
M _i , S _i , BI _b , M _b , S _b	2,0	2,0	2,0	4,0	3,0	2,5

1.2.11.3 Polar ships shall have a minimum corrosion/abrasion addition of $t_s = 1,0$ mm applied to all internal structures within the ice-strengthened hull areas, including plated members adjacent to the shell, as well as stiffener webs and flanges.

1.2.11.4 Steel renewal for ice strengthened structures is required when the gauged thickness is less than $t_{net} + 0,5$ mm.

1.2.12 Materials.

1.2.12.1 Plating materials for hull structures shall be not less than those given in Tables 1.2.12.4 and 1.2.12.5 based on the as-built thickness of the material, the polar ice class notation assigned to the ship and the material class of structural members according to 1.2.12.2.

1.2.12.2 Material classes specified in Table 1.2.3.7-1, Part II "Hull" are applicable to polar ships regardless of the ship's length. In addition, material classes for weather and sea exposed structural members and for members attached to the weather and sea exposed shell plating of polar ships are given in Table 1.2.12.1. Where the material classes in Table 1.2.12.1 and those in Table 1.2.3.7-1, Part II "Hull" differ, the higher material class shall be applied.

1.2.12.3 Steel grades for all plating and attached framing of hull structures and appendages situated below the level of 0,3 m below the lower waterline, as shown in Figure 1.2.12.3, shall be obtained from Table 1.2.3.7-2, Part II "Hull" based on the material class for structural members in Table 1.2.12.1 above, regardless of polar class.

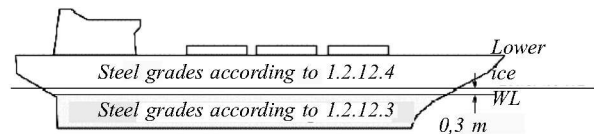


Fig. 1.2.12.3

Steel grade requirements for submerged and weather exposed shell plating

1.2.12.4 Steel grades for all weather exposed plating of hull structures and appendages situated above the level of 0,3 m below the lower ice waterline, as shown in Fig. 1.2.12.3, shall be not less than given in Table 1.2.12.4.

1.2.12.5 Steel grades for all inboard framing members attached to weather exposed plating shall be not less than given in Table 1.2.12.5. This applies to all

Table 1.2.12.1

Material classes for structural members of polar ships

Structural members	Material class
Shell plating within the bow and bow intermediate ice belt hull areas (B, BI _i)	II
All weather and sea exposed secondary and primary (as defined in Table 1.2.3.7-1, Part II "Hull") structural members outside 0,4L amidships	I
Plating materials for stem and stern frames, rudder horn, rudder, propeller nozzle, shaft brackets, ice skeg, ice knife and other appendages subject to ice impact loads	II
All inboard framing members attached to the weather and sea-exposed plating including any contiguous inboard member within 600 mm of the shell plating	I
Weather-exposed plating and attached framing in cargo holds of ships which by nature of their trade have their cargo hold hatches open during cold weather operations	I
All weather and sea exposed special (as defined in Table 1.2.3.7-1, Part II "Hull") structural members within 0,2L from FP	II

Table 1.2.12.4

Steel grades for weather exposed plating

Thickness t , mm	Material Class I				Material Class II				Material Class III					
	PC1 to PC5		PC6 and PC7		PC1 to PC5		PC6 and PC7		PC1 to PC3		PC4 and PC5		PC6 and PC7	
	MS	HT	MS	HT	MS	HT	MS	HT	MS	HT	MS	HT	MS	HT
$t \leq 10$	B	AH	B	AH	B	AH	B	AH	E	EH	E	EH	B	AH
$10 < t \leq 15$	B	AH	B	AH	D	DH	B	AH	E	EH	E	EH	D	DH
$15 < t \leq 20$	D	DH	B	AH	D	DH	B	AH	E	EH	E	EH	D	DH
$20 < t \leq 25$	D	DH	B	AH	D	DH	B	AH	E	EH	E	EH	D	DH
$25 < t \leq 30$	D	DH	B	AH	E	EH2	D	DH	E	EH	E	EH	E	EH
$30 < t \leq 35$	D	DH	B	AH	E	EH	D	DH	E	EH	E	EH	E	EH
$35 < t \leq 40$	D	DH	D	DH	E	EH	D	DH	F	FH	E	EH	E	EH
$40 < t \leq 45$	E	EH	D	DH	E	EH	D	DH	F	FH	E	EH	E	EH
$45 < t \leq 50$	E	EH	D	DH	E	EH	D	DH	F	FH	F	FH	E	EH

Notes: 1. Includes weather-exposed plating of hull structures and appendages, as well as their outboard framing members, situated above a level of 0,3 m below the lowest ice waterline.
2. Grades D, DH are allowed for a single strake of side shell plating not more than 1,8 m wide from 0,3 m below the lowest ice waterline.

Table 1.2.12.5

Steel grades for inboard framing members attached to weather exposed plating

Thickness t , mm	PC1 to PC5		PC6 and PC7	
	MS	HT	MS	HT
$t \leq 20$	B	AH	B	AH
$20 < t \leq 35$	D	DH	D	AH
$35 < t \leq 45$	D	DH	D	DH
$45 < t \leq 50$	E	EH	E	DH

inboard framing members as well as to other contiguous inboard members (e.g. bulkheads, decks) within 600 mm of the exposed plating.

1.2.12.6 Castings shall have specified properties consistent with the expected service temperature for the cast component.

1.2.13 Longitudinal strength.

1.2.13.1 Application.

1.2.13.1.1 Ice loads need only be combined with still water loads. The combined stresses shall be compared against permissible bending and shear stresses at different locations along the ship's length. In addition, sufficient local buckling strength shall also be verified.

1.2.13.2 Design vertical ice force at the bow.

1.2.13.2.1 The design vertical ice force at the bow F_{IB} , MN, shall be taken as:

$$F_{IB} = \min(F_{IB,1}; F_{IB,2}) \quad (1.2.13.2.1-1)$$

$$\text{where } F_{IB,1} = 0,534K_1^{0,15} \sin^{0,2}(\gamma_{stem}) (DK_h)^{0,5} CF_L; \quad (1.2.13.2.1-2)$$

$$F_{IB,2} = 1,20CF_F; \quad (1.2.13.2.1-3)$$

K_L = indentation parameter = K_f / K_h ;

.1 for the case of a blunt bow form:

$$K_f = (2CB^{1-eb}/(1+eb))^{0,9} \tan(\gamma_{stem})^{-0,9(1+eb)};$$

.2 for the case of wedge bow form ($\alpha_{stem} < 80^\circ$), $e_b = 1$ and the above simplifies to:

$$K_f = (\tan(\alpha_{stem})/\tan^2(\gamma_{stem}))^{0,9};$$

$$K_h = 0,01A_{wp}, \text{ MN/m};$$

CF_L = longitudinal strength class factor from Table 1.2.3.2.1;

e_b = bow shape exponent which best describes the waterplane (refer to Figs. 1.2.13.2.1-1 and 1.2.13.2.1-2);

$e_b = 1,0$ for a simple wedge bow form;

$e_b = 0,4$ to $0,6$ for a spoon bow form;

$e_b = 0$ for a landing craft bow form;

an approximate e_b determined by a simple fit is acceptable;

γ_{stem} = stem angle to be measured between the horizontal axis and the stem tangent at the upper ice waterline, deg. (buttock angle as per Fig. 1.2.3.2.1.1.1 measured on the centreline);

α_{stem} = waterline angle measured in way of the stem at the upper ice waterline (UIWL), in deg. (refer to Figure 1.2.13.2.1-1);

$$C = 1/(2(L_B/B)^{e_b});$$

B = ship moulded breadth, m;

L_B = bow length used in the equation $y = B/2(x/L_B)^{e_b}$, m (refer to Figs 1.2.13.2.1-1 and 1.2.13.2.1-2);

D = ship displacement, kt, not to be taken less than 10 kt;

A_{wp} = ship waterplane area, m²;

CF_F = flexural failure class factor from Table 1.2.3.2.1.

Where applicable, draught dependent quantities shall be determined at the waterline corresponding to the loading condition under consideration.

1.2.13.3 Design vertical shear force.

1.2.13.3.1 The design vertical ice shear force F_I , MN, along the hull girder shall be determined by the formula

$$F_I = C_f F_{IB} \quad (1.2.13.3.1)$$

where C_f = longitudinal distribution factor to be taken as follows:

.1 positive shear force:

$C_f = 0,0$ between the aft end of L and $0,6L$ from aft;

$C_f = 1,0$ between $0,9L$ from aft and the forward end of L ;

.2 negative shear force:

$C_f = 0,0$ at the aft end of L ;

$C_f = -0,5$ between $0,2L$ and $0,6L$ from aft;

$C_f = 0,0$ between $0,8L$ from aft and the forward end of L .

Intermediate values shall be determined by linear interpolation.

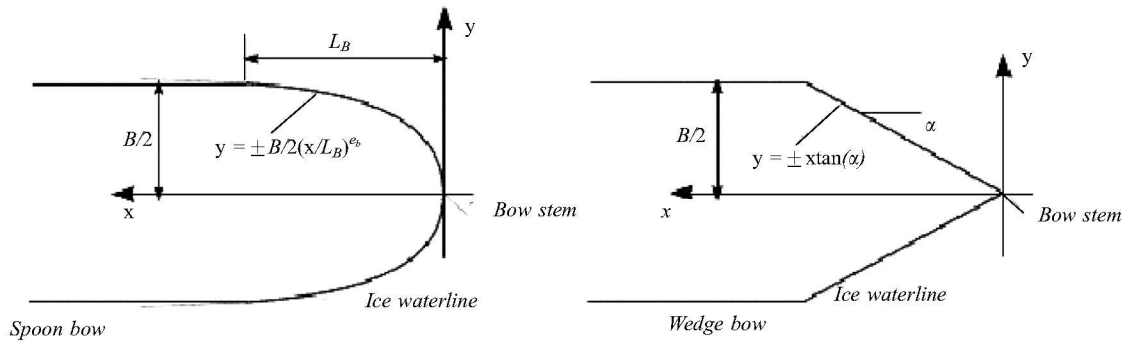


Fig. 1.2.13.2.1-1
Bow shape definition

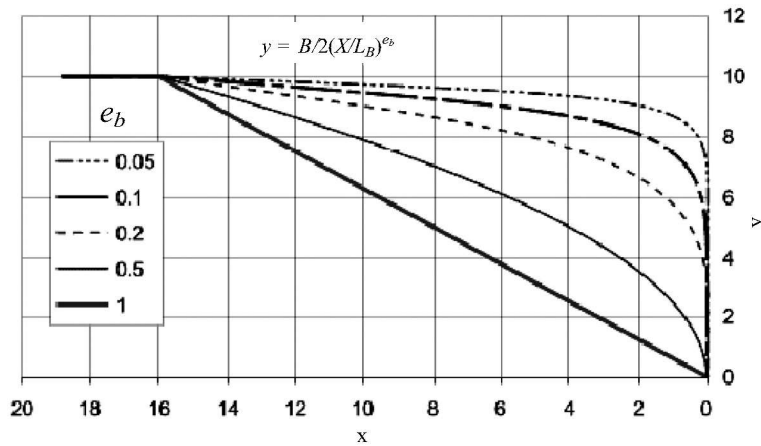


Fig. 1.2.13.2.1-2
Illustration of e_b effect on the bow shape for $B = 20$ and $L_B = 16$

1.2.13.3.2 The applied vertical shear stress τ_a shall be determined along the hull girder in a similar manner as in 1.6.5.1, Part II "Hull" by substituting the design vertical ice shear force for the design vertical wave shear force.

1.2.13.4 Design vertical ice bending moment.

1.2.13.4.1 The design vertical ice bending moment M_I , MNm, along the hull girder shall be determined by the formula

$$M_I = 0,1 C_m L \sin^{-0,2}(\gamma_{stem}) F_{IB} \quad (1.2.13.4.1)$$

where L = ship length (length as defined in 1.1.3, Part II "Hull"), m;

γ_{stem} as given in 1.2.13.2.1;

F_{IB} = design vertical ice force at the bow, MN;

C_m = longitudinal distribution factor for design vertical ice bending moment to be taken as follows:

$C_m = 0,0$ at the aft end of L ;

$C_m = 1,0$ between $0,5L$ and $0,7L$ from aft;

$C_m = 0,3$ at $0,95L$ from aft;

$C_m = 0,0$ at the forward end of L .

Intermediate values shall be determined by linear interpolation. Where applicable, draught dependent quantities shall be determined at the waterline corresponding to the loading condition under consideration.

1.2.13.4.2 The applied vertical bending stress σ_a shall be determined along the hull girder in a similar manner as in 1.6.5.1, Part II "Hull" by substituting the

design vertical ice bending moment for the design vertical wave bending moment. The ship still water bending moment shall be taken as the maximum sagging moment.

1.2.13.5 Longitudinal strength criteria.

1.2.13.5.1 The strength criteria provided in Table 1.2.13.5.1 shall be satisfied. The design stress is not to exceed the permissible stress.

1.2.14 Stem and stern frames.

1.2.14.1 The stem and stern frame shall be designed according to the Register requirements. For PC6 and PC7 ships requiring 1AS and 1A equivalency, the stem and stern requirements of the Finnish-Swedish Ice Class Rules may need to be additionally considered.

1.2.15 Appendages.

1.2.15.1 All appendages shall be designed to withstand forces appropriate for the location of their attachment to the hull structure or their position within a hull area.

1.2.15.2 Load definition and response criteria shall be determined by the Register.

1.2.16 Local details.

1.2.16.1 For the purpose of transferring ice-induced loads to supporting structure (bending moments and

Table 1.2.13.5.1

Longitudinal strength criteria

Failure mode	Applied stress	Permissible stress when $\sigma_y/\sigma_u \leq 0,7$	Permissible stress when $\sigma_y/\sigma_u > 0,7$
Tension	σ_a	$\eta \sigma_y$	$\eta 0,41(\sigma_u + \sigma_y)$
Shear	τ_a	$\eta \sigma_y/3^{0,5}$	$\eta 0,41(\sigma_u + \sigma_y)/3^{0,5}$
Buckling	σ_a	σ_c for plating and for web plating of stiffeners $\sigma_c/1,1$ for stiffeners	
	τ_a	τ_c	
where σ_a = applied vertical bending stress, N/mm ² ; τ_a = applied vertical shear stress, N/mm ² ; σ_y = minimum upper yield stress of the material, N/mm ² ; σ_u = ultimate tensile strength of material, N/mm ² ; σ_c = critical buckling stress in compression, according to 1.6.5.3, Part II "Hull", N/mm ² ; τ_c = critical buckling stress in shear, according to 1.6.5.3, Part II "Hull", N/mm ² ; $\eta = 0,8$.			

shear forces), local design details shall comply with the Register requirements.

1.2.16.2 The loads carried by a member in way of cut-outs shall not cause instability. Where necessary, the structure shall be stiffened.

1.2.17 Direct calculations.

1.2.17.1 Direct calculations shall not be utilised as an alternative to the analytical procedures prescribed in the present Chapter.

1.2.17.2 Where direct calculation is used to check the strength of structural systems, the load patch specified in 1.2.3 shall be applied.

1.2.18 Welding.

1.2.18.1 All welding within ice-strengthened areas shall be of the double continuous type.

1.2.18.2 Continuity of strength shall be ensured at all structural connections.

**1.3 MACHINERY REQUIREMENTS
FOR POLAR CLASS SHIPS**

1.3.1 Application.

The requirements of this Chapter apply to main propulsion, steering gear, emergency and essential auxiliary systems essential for the safety of the ship and the survivability of the crew.

1.3.2 General.

1.3.2.1 Drawings and particulars to be submitted:

1 details of the environmental conditions and the required ice class for the machinery, if different from ship's ice class;

2 detailed drawings of the main propulsion machinery. Description of the main propulsion, steering, emergency and essential auxiliaries shall include operational limitations. Information on essential main propulsion load control functions;

3 description detailing how main, emergency and auxiliary systems are located and protected to prevent problems from freezing, ice and snow and evidence of

their capability to operate in intended environmental conditions;

4 calculations and documentation indicating compliance with the requirements of this Chapter.

1.3.2.2 System design.

1.3.2.2.1 Machinery and supporting auxiliary systems shall be designed, constructed and maintained to comply with the requirements of periodically unmanned machinery spaces with respect to fire safety. Any automation plant (i.e. control, alarm, safety and indication systems) for essential systems installed shall be maintained to the same standard.

1.3.2.2.2 Systems, subject to damage by freezing, shall be drainable.

1.3.2.2.3 Single screw vessels classed **PC1** to **PC5** inclusive shall have means provided to ensure sufficient ship operation in the case of propeller damage including CP-mechanism.

1.3.3 Materials.

1.3.3.1 Materials exposed to sea water.

Materials exposed to sea water, such as propeller blades, propeller hub and blade bolts shall have an elongation not less than 15 per cent on a test piece the length of which is five times the diameter.

Charpy V-notch impact test (determination of impact energy KV for sharply-notched specimen) shall be carried out for other than bronze and austenitic steel materials. Test pieces taken from the propeller castings shall be representative of the thickest section of the blade. An average impact energy KV value of 20 J taken from three Charpy V-notch tests shall be obtained at minus 10 °C.

1.3.3.2 Materials exposed to sea water temperature.

Materials exposed to sea water temperature shall be of steel or other approved ductile material. An average impact energy KV value of 20 J taken from three tests shall be obtained at minus 10 °C.

1.3.3.3 Material exposed to low air temperature.

Materials of essential components exposed to low air temperature shall be of steel or other approved ductile material.

An average impact energy KV value of 20 J taken from three Charpy V-notch tests shall be obtained at 10 °C below the lowest design temperature.

1.3.4 Ice interaction load.

1.3.4.1 Propeller ice interaction.

The present requirements cover open and ducted type propellers situated at the stern of a ship having controllable pitch or fixed pitch blades. Ice loads on bow propellers and pulling type propellers shall receive special consideration by the Register.

The given loads are expected, single occurrence, maximum values for the whole ships service life for normal operational conditions.

These loads do not cover off-design operational conditions, for example when a stopped propeller is dragged through ice.

The present requirements considering loads due to propeller ice interaction apply also for azimuthing (geared and podded) thrusters. However, ice loads due to ice impacts on the body of azimuthing thrusters are not covered by the present Section.

The loads given in 1.3.4 are total loads (unless otherwise stated) during ice interaction and shall be applied separately (unless otherwise stated) and are intended for component strength calculations only. The different loads given here shall be applied separately.

F_b is a force bending a propeller blade backwards when the propeller mills an ice block while rotating ahead.

F_f is a force bending a propeller blade forwards when a propeller interacts with an ice block while rotating ahead.

1.3.4.2 Ice class factors.

The Table 1.3.4.2 below lists the design ice thickness and ice strength index to be used for estimation of the propeller ice loads.

Table 1.3.4.2

Ice class	H_{ice} , m	S_{ice}	S_{qice}
PC1	4,0	1,2	1,15
PC2	3,5	1,1	1,15
PC3	3,0	1,1	1,15
PC4	2,5	1,1	1,15
PC5	2,0	1,1	1,15
PC6	1,75	1	1
PC7	1,5	1	1

where H_{ice} = ice thickness for machinery strength design;
 S_{ice} = ice strength index for blade ice force;
 S_{qice} = ice strength index for blade ice torque.

1.3.4.3 Design ice loads for open propeller.

1.3.4.3.1 Maximum backward blade force F_b , kN:

when $D < D_{limit}$:

$$F_b = -27S_{ice}[nD]^{0,7}[EAR/Z]^{0,3}[D]^2; \quad (1.3.4.3.1-1)$$

when $D \geq D_{limit}$:

$$F_b = -23S_{ice}[nD]^{0,7}[EAR/Z]^{0,3}(H_{ice})^{1,4}[D]^2 \quad (1.3.4.3.1-2)$$

where $D_{limit} = 0,85(H_{ice})^{1,4}$,

n is the nominal rotational speed (at MCR free running condition) for CP-propeller and 85 per cent of the nominal rotational speed (at MCR free running condition) for a FP-propeller (regardless driving engine type).

F_b shall be applied as a uniform pressure distribution to an area on the back (suction) side of the blade for the following load cases:

.1 load case 1: from 0,6R to the tip and from the blade leading edge to a value of 0,2 chord length;

.2 load case 2: a load equal to 50 per cent of the F_b shall be applied on the propeller tip area outside of 0,9R;

.3 load case 5: for reversible propellers a load equal to 60 per cent of the F_b shall be applied from 0,6R to the tip and from the blade trailing edge to a value of 0,2 chord length.

Refer to load cases 1, 2 and 5 in Table 1 of the Appendix.

1.3.4.3.2 Maximum forward blade force F_f , kN:

when $D < D_{limit}$:

$$F_f = 250[EAR/Z][D]^2; \quad (1.3.4.3.2-1)$$

when $D \geq D_{limit}$:

$$F_f = 500 \frac{1}{(1 - \frac{d}{D})} H_{ice}[EAR/Z][D]^2 \quad (1.3.4.3.2-2)$$

where

$$D_{limit} = \frac{2}{(1 - \frac{d}{D})} H_{ice}; \quad (1.3.4.3.2-3)$$

d = propeller hub diameter, m;

D = propeller diameter, m;

EAR = expanded blade area ratio;

Z = number of propeller blades.

F_f shall be applied as a uniform pressure distribution to an area on the face (pressure) side of the blade for the following loads cases:

.1 load case 3: from 0,6R to the tip and from the blade leading edge to a value of 0,2 chord length;

.2 load case 4: a load equal to 50 per cent of the F_f shall be applied on the propeller tip area outside of 0,9R;

.3 load case 5: for reversible propellers a load equal to 60 per cent F_f shall be applied from 0,6R to the tip and from the blade trailing edge to a value of 0,2 chord length.

Load cases 3, 4 and 5 — refer to Table 1 of the Appendix.

1.3.4.3.3 Maximum blade spindle torque Q_{Smax} .

Spindle torque Q_{Smax} , kNm, around the spindle axis of the blade fitting shall be calculated both for the load cases described in 1.3.4.3.1 and 1.3.4.3.2 for F_b and F_f . If these spindle torque values are less than the default value given below, the default minimum value shall be used. Default value:

$$Q_{Smax} = 0,25Fc_{0,7} \quad (1.3.4.3.3)$$

where $c_{0,7}$ = length of the blade chord at 0,7R radius, m;

F is either F_b or F_f which ever has the greater absolute value.

1.3.4.3.4 Maximum propeller ice torque applied to the propeller Q_{\max} , kNm:

when $D < D_{\text{limit}}$:

$$Q_{\max} = 105(1-d/D)S_{\text{gice}}(P_{0,7}/D)^{0,16}(t_{0,7}/D)^{0,6}(nD)^{0,17}D^3; \quad (1.3.4.3.4-1)$$

when $D \geq D_{\text{limit}}$:

$$Q_{\max} = 202(1-d/D)S_{\text{gice}}H_{\text{ice}}^{1,1}(P_{0,7}/D)^{0,16}(t_{0,7}/D)^{0,6}(nD)^{0,17}D^{1,9} \quad (1.3.4.3.4-2)$$

where $D_{\text{limit}} = 1,8H_{\text{ice}}$;

S_{gice} = ice strength index for blade ice torque;

$P_{0,7}$ = propeller pitch at 0,7R, m;

$t_{0,7}$ = max thickness at 0,7R, m;

n is the rotational propeller speed, rps, at bollard condition. If not known, n shall be taken according to Table 1.3.4.3.4.

Table 1.3.4.3.4

Propeller type	n
CP propellers	n_n
FP propellers driven by turbine or electric motor	n_n
FP propellers driven by diesel engine	$0,85n_n$
where n_n is the nominal rotational speed at MCR, free running condition.	

For CP propellers, propeller pitch $P_{0,7}$ shall correspond to MCR in bollard condition. If not known, $P_{0,7}$ shall be taken as $0,7P_{0,7n}$, where $P_{0,7n}$ is propeller pitch at MCR free running condition.

1.3.4.3.5 Maximum propeller ice thrust applied to the shaft:

$$T_f = 1,1F_f; \quad (1.3.4.3.5-1)$$

$$T_b = 1,1F_b. \quad (1.3.4.3.5-2)$$

1.3.4.4 Design ice loads for ducted propeller.

1.3.4.4.1 Maximum backward blade force F_b :

where $D < D_{\text{limit}}$:

$$F_b = -9,5S_{\text{ice}}(EAR/Z)^{0,3}(nD)^{0,7}D^2; \quad (1.3.4.4.1-1)$$

where $D \geq D_{\text{limit}}$:

$$F_b = -66S_{\text{ice}}(EAR/Z)^{0,3}(nD)^{0,7}(H_{\text{ice}})^{1,4}D^{0,6} \quad (1.3.4.4.1-2)$$

where $D_{\text{limit}} = 4H_{\text{ice}}$;

n shall be taken as in 1.3.4.3.1.

F_b shall be applied as a uniform pressure distribution to an area on the back side for the following load cases (refer to Table 2 of the Appendix):

1 load case 1: on the back of the blade from 0,6R to the tip and from the blade leading edge to a value of 0,2 chord length;

2 load case 5: for reversible rotation propellers a load equal to 60 per cent of F_b is applied on the blade face from 0,6R to the tip and from the blade trailing edge to a value of 0,2 chord length.

1.3.4.4.2 Maximum forward blade force F_f , kN:

when $D < D_{\text{limit}}$:

$$F_f = 250(EAR/Z)D^2; \quad (1.3.4.4.2-1)$$

when $D \geq D_{\text{limit}}$:

$$F_f = 500 \frac{1}{(1-\frac{d}{D})} H_{\text{ice}}[EAR/Z][D]^2 \quad (1.3.4.4.2-2)$$

$$\text{where } D_{\text{limit}} = \frac{2}{(1-\frac{d}{D})} H_{\text{ice}}, \text{ m.} \quad (1.3.4.4.2-3)$$

F_f shall be applied as a uniform pressure distribution to an area on the face (pressure) side for the following load case (refer to Table 2 of the Appendix):

1 load case 3: on the blade face from 0,6R to the tip and from the blade leading edge to a value of 0,5 chord length;

2 load case 5: a load equal to 60 per cent F_f shall be applied from 0,6R to the tip and from the blade leading edge to a value of 0,2 chord length.

1.3.4.4.3 Maximum propeller ice torque applied to the propeller Q_{\max} , kNm, is the maximum torque on a propeller due to ice-propeller interaction:

when $D \leq D_{\text{limit}}$:

$$Q_{\max} = 74(1-d/D)S_{\text{gice}}(P_{0,7}/D)^{0,16}(t_{0,7}/D)^{0,6}(nD)^{0,17}D^3; \quad (1.3.4.4.3-1)$$

when $D \geq D_{\text{limit}}$:

$$Q_{\max} = 141(1-d/D)S_{\text{gice}}H_{\text{ice}}^{1,1}(P_{0,7}/D)^{0,16}(t_{0,7}/D)^{0,6}(nD)^{0,17}D^{1,9} \quad (1.3.4.4.3-2)$$

where $D_{\text{limit}} = 1,8H_{\text{ice}}$, m;

n is the rotational propeller speed, rps, at bollard condition.

If not known, n shall be taken according to Table 1.3.4.4.3.

Таблица 1.3.4.4.3

Propeller type	n
CP propellers	n_n
FP propellers driven by turbine or electric motor	n_n
FP propellers driven by diesel engine	$0,85n_n$
where n_n is the nominal rotational speed at MCR, free running condition.	

For CP propellers, propeller pitch $P_{0,7}$ shall correspond to MCR in bollard condition. If not known, $P_{0,7}$ shall be taken as $0,7P_{0,7n}$, where $P_{0,7n}$ is propeller pitch at MCR free running condition.

1.3.4.4.4 Maximum blade spindle torque for CP-mechanism design Q_{smax} .

Spindle torque Q_{smax} , kNm, around the spindle axis of the blade fitting shall be calculated for the load case described in 1.3.4.1. If these spindle torque values are less than the default value given below, the default value shall be used.

Default value:

$$Q_{smax} = 0,25Fc_{0,7} \quad (1.3.4.4.4)$$

where $c_{0,7}$ the length of the blade section at $0,7R$ radius;
 F is either F_b or F_f whichever has the greater absolute value.

1.3.4.4.5 Maximum propeller ice thrust (applied to the shaft at the location of the propeller):

Maximum forward propeller ice thrust:

$$T_f = 1,1F_f. \quad (1.3.4.4.5-1)$$

Maximum backward propeller ice thrust:

$$T_b = 1,1F_b. \quad (1.3.4.4.5-2)$$

1.3.4.5 Reserved.

1.3.4.6 Design loads on propulsion line.

1.3.4.6.1 Torque.

The propeller ice torque excitation for shaft line dynamic analysis shall be described by a sequence of blade impacts which are of half sine shape and occur at the blade. The torque due to a single blade ice impact as a function of the propeller rotation angle is then:

$$Q(\varphi) = C_q Q_{max} \sin(\varphi(180/\alpha_i)) \text{ when } \varphi = 0 \dots \alpha_i;$$

$$Q(\varphi) = 0 \text{ when } \varphi = \alpha_i \dots 360. \quad (1.3.4.6.1-1)$$

C_q and α_i parameters are given in Table 1.3.4.6.1.

Table 1.3.4.6.1

Torque excitation	Propeller-ice interaction	C_q	α_i
Case 1	Single ice block	0,5	45
Case 2	Single ice block	0,75	90
Case 3	Single ice block	1,0	135
Case 4	Two ice blocks with 45 degree phase in rotation angle	0,5	45

The total ice torque is obtained by summing the torque of single blades taking into account the phase shift $360 \text{ deg}/Z$. The number of propeller revolutions during a milling sequence shall be determined by the formula

$$N_Q = 2H_{ice}. \quad (1.3.4.6.1-2)$$

The number of impacts is ZN_Q (refer to Fig. 1 in the Appendix).

Milling torque sequence duration is not valid for pulling bow propellers, which are subject to special consideration by the Register in each particular case.

The response torque at any shaft component shall be analysed considering excitation torque $Q(\varphi)$ at the propeller, actual engine torque Q_e and mass elastic system.

Q_e = actual maximum engine torque at considered speed.

Design torque along propeller shaft line.

The design torque Q_r of the shaft component shall be determined by means of torsional vibration analysis of the propulsion line. Calculations shall be carried out for all excitation cases given above and the response shall be

applied on top of the mean hydrodynamic torque in bollard condition at considered propeller rotational speed.

1.3.4.6.2 Maximum response thrust (maximum thrust along the propeller shaft line).

Maximum thrust along the propeller shaft line shall be calculated with the formulae below. The factors 2,2 and 1,5 take into account the dynamic magnification due to axial vibration. Alternatively the propeller thrust magnification factor may be calculated by dynamic analysis.

Maximum shaft thrust forwards, kN:

$$T_r = T_n + 2,2T_f. \quad (1.3.4.6.2-1)$$

Maximum shaft thrust backwards, kN:

$$T_r = 1,5T_b \quad (1.3.4.6.2-2)$$

where T_n = propeller bollard thrust, kN;

T_f = maximum forward propeller ice thrust, kN;

T_b = maximum backward propeller ice thrust, kN.

If hydrodynamic bollard thrust T_n is not known, T_n shall be taken according to Table 1.3.4.6.2.

Table 1.3.4.6.2

Propeller type	T_n
CP propellers (open)	1,25T
CP propellers (ducted)	1,1T
FP propellers driven by turbine or electric motor	T
FP propellers driven by diesel engine (open)	0,85T
FP propellers driven by diesel engine (ducted)	0,75T

where T = nominal propeller thrust at MCR at free running open water conditions.

1.3.4.6.3 Blade failure load for both open and nozzle propeller.

The force is acting at $0,8R$ in the weakest direction of the blade and at a spindle arm of $2/3$ of the distance of axis of blade rotation of leading and trailing edge which ever is the greatest.

The blade failure load F_{ex} , kN, is determined by the formula

$$F_{ex} = \frac{0,3ct^2\sigma_{ref}}{0,8D-2r} \cdot 10^3 \quad (1.3.4.6.3)$$

where $\sigma_{ref} = 0,6\sigma_{0,2} + 0,4\sigma_u$;

σ_u and $\sigma_{0,2}$ are representative values for the blade material;

c , t and r are respectively the actual chord length, thickness and radius of the cylindrical root section of the blade at the weakest section outside root fillet, and typically will be at the termination of the fillet into the blade profile.

1.3.5 Design.

1.3.5.1 Design principle.

The strength of the propulsion line shall be designed: for maximum loads in 1.3.4;

such that the plastic bending of a propeller blade shall not cause damages in other propulsion line components; with sufficient fatigue strength.

1.3.5.2 Azimuthing main propulsors.

In addition to the above requirements special consideration shall be given to the loading cases which

are extraordinary for propulsion units when compared with conventional propellers. Estimation of the loading cases shall reflect the operational realities of the ship and the thrusters. In this respect, for example, the loads caused by impacts of ice blocks on the propeller hub of a pulling propeller shall be considered. Also loads due to thrusters operating in an oblique angle to the flow shall be considered. The steering mechanism, the fitting of the unit and the body of the thruster shall be designed to withstand the loss of a blade without damage. The plastic bending of a blade shall be considered in the propeller blade position, which causes the maximum load on the studied component.

Azimuth thrusters shall also be designed for estimated loads due to thruster body/ice interaction as per 1.2.15.

1.3.5.3 Blade design.

1.3.5.3.1 Maximum blade stresses.

Blade stresses shall be calculated using the backward and forward loads given in section 1.3.4.3 and 1.3.4.4. The stresses shall be calculated with recognised and well-documented FE-analysis or other acceptable alternative method.

The stresses on the blade shall not exceed the allowable stresses σ_{all} for the blade material given below.

Calculated blade stress for maximum ice load shall comply with the following:

$$\sigma_{calc} < \sigma_{all} = \sigma_{ref} / S \quad (1.3.5.3.1-1)$$

where $S = 1,5$;

σ_{ref} = reference stress, defined as:

$$\sigma_{ref} = 0,7\sigma_u; \text{ or} \quad (1.3.5.3.1-2)$$

$$\sigma_{ref} = 0,6\sigma_{0,2} + 0,4\sigma_u, \text{ whichever is less,} \quad (1.3.5.3.1-3)$$

where σ_u and $\sigma_{0,2}$ = representative values for the blade material.

1.3.5.3.2 Blade edge thickness.

The blade edge thicknesses t_{edge} and t_{tip} thickness t_{tip} shall be greater than t_{edge} determined by the formula the following formula

$$t_{edge} \geq x S S_{ice} \sqrt{3 p_{ice} / \sigma_{ref}} \quad (1.3.5.3.2)$$

where x = distance from the blade edge measured along the cylindrical sections from the edge and shall be 2,5 per cent of chord length, however not to be taken greater than 45 mm. In the tip area (above 0,975R) x shall be taken as 2,5 per cent of 0,975R section length and shall be measured perpendicularly to the edge, however not to be taken greater than 45 mm;

S = safety factor;

$S = 2,5$ for trailing edges;

$S = 3,5$ for leading edges;

$S = 5$ for tip;

S_{ice} = according to 1.3.4.2;

p_{ice} = ice pressure;

$p_{ice} = 16$ MPa for leading edge and tip thickness;

σ_{ref} = according to 1.3.5.3.1.

The requirement for edge thickness shall be applied for leading edge and in case of reversible rotation open propellers also for trailing edge. Tip thickness refers to the maximum measured thickness in the tip area above 0,975R. The edge thickness in the area between position

of maximum tip thickness and edge thickness at 0,975R shall be interpolated between edge and tip thickness value and smoothly distributed.

1.3.5.3.3 to 1.3.5.4.2 Reserved.

1.3.5.5 Reserved.

1.3.5.6 Prime movers.

1.3.5.6.1 The main engine shall be capable of being started and running the propeller with the CP in full pitch.

1.3.5.6.2 Provisions shall be made for heating arrangements to ensure ready starting of the cold emergency power units at an ambient temperature applicable to the polar class of the ship.

1.3.5.6.3 Emergency power units shall be equipped with starting devices with a stored energy capability of at least three consecutive starts at the design temperature in 1.3.5.6.2 above. The source of stored energy shall be protected to preclude critical depletion by the automatic starting system, unless a second independent means of starting is provided. A second source of energy shall be provided for an additional three starts within 30 min, unless manual starting can be demonstrated to be effective.

1.3.6 Machinery fastening loading accelerations.

1.3.6.1 Essential equipment and main propulsion machinery supports shall be suitable for the accelerations as indicated in as follows. Accelerations shall be considered acting independently.

1.3.6.2 Longitudinal impact accelerations a_l .

Maximum longitudinal impact acceleration at any point along the hull girder, m/s^2 , is determined by the formula

$$a_l = (F_{IB}/\Delta) \{ [1,1 \tan(\gamma + \varphi)] + [7H/L] \}, \quad (1.3.6.2)$$

where φ = maximum friction angle between steel and ice, normally taken as 10 deg.;

γ = bow stem angle at waterline, deg.;

Δ = displacement;

L = length between perpendiculars, m;

H = distance from the waterline to the point being considered, m;

F_{IB} = vertical impact force, defined in 1.2.13.2.1;

F_i = total force normal to shell plating in the bow area due to oblique ice impact, defined in 1.2.3.2.1.

1.3.6.3 Vertical acceleration a_v .

Combined vertical impact acceleration at any point along the hull girder, m/s^2 , is determined by the formula

$$a_v = 2,5 (F_{IB}/\Delta) F_x \quad (1.3.6.3)$$

where $F_x = 1,3$ at FP;

$F_x = 0,2$ at midships;

$F_x = 0,4$ at AP;

$F_x = 1,3$ at AP for ships conducting ice breaking astern.

Intermediate values to be interpolated linearly.

1.3.6.4 Transverse impact acceleration a_t .

Combined transverse impact acceleration at any point along hull girder, m/s^2 , is determined by the formula

$$a_t = 3 F_i F_x / \Delta \quad (1.3.6.4)$$

where $F_x = 1,5$ at FP;

$F_x = 0,25$ at midships;

$F_x = 0,5$ at AP;

$F_x = 1,5$ at AP for ships conducting ice breaking astern.

Intermediate values to be interpolated linearly.

1.3.7 Auxiliary systems.

1.3.7.1 Machinery shall be protected from the harmful effects of ingestion or accumulation of ice or snow. Where continuous operation is necessary, means shall be provided to purge the system of accumulated ice or snow.

1.3.7.2 Means shall be provided to prevent damage due to freezing, to tanks containing liquids.

1.3.7.3 Vent pipes, intake and discharge pipes and associated systems shall be designed to prevent blockage due to freezing or ice and snow accumulation.

1.3.8 Sea inlets and cooling water systems.

1.3.8.1 Cooling water systems for machinery that are essential for the propulsion and safety of the vessel, including sea chests inlets, shall be designed for the environmental conditions applicable to the ice class.

1.3.8.2 At least two sea chests shall be arranged as ice boxes for class **PC1** to **PC5** ships. The calculated volume for each of the ice boxes shall be at least 1 m^3 for every 750 kW of the total installed power. For **PC6** and **PC7** there shall be at least one icebox located preferably near centre line.

1.3.8.3 Ice boxes shall be designed for an effective separation of ice and venting of air.

1.3.8.4 Sea inlet valves shall be secured directly to the ice boxes. The valve shall be a full bore type.

1.3.8.5 Ice boxes and sea chests shall have vent pipes and shall have shut off valves connected direct to the shell.

1.3.8.6 Means shall be provided to prevent freezing of sea chests, ice boxes, ship side valves and fittings above the load waterline.

1.3.8.7 Efficient means shall be provided to re-circulate cooling seawater to the ice box. Total sectional area of the circulating pipes shall not be less than the area of the cooling water discharge pipe.

1.3.8.8 Detachable gratings or manholes shall be provided for ice boxes. Manholes shall be located above the deepest load line. Access shall be provided to the ice box from above.

1.3.8.9 Openings in ship sides for ice boxes shall be fitted with gratings, or holes or slots in shell plates. The net area through these openings shall be not less than 5 times the area of the inlet pipe. The diameter of holes and width of slot in shell plating shall be not less than 20 mm. Gratings of the ice boxes shall be provided with a means of clearing. Clearing pipes shall be provided with screw-down type non return valves.

1.3.9 Ballast tanks.

1.3.9.1 Efficient means shall be provided to prevent freezing in fore and after peak tanks and wing tanks located above the water line and where otherwise found necessary.

1.3.10 Ventilation system.

1.3.10.1 The air intakes for machinery and accommodation ventilation shall be located on both sides of the ship.

1.3.10.2 Accommodation and ventilation air intakes shall be provided with means of heating.

1.3.10.3 The temperature of inlet air provided to machinery from the air intakes shall be suitable for the safe operation of the machinery.

1.3.11 Reserved.

1.3.12 Alternative design.

1.3.12.1 As an alternative — a comprehensive design study may be submitted and may be requested to be validated by an agreed test programme.

APPENDIX

Table 1

Load cases for open propeller

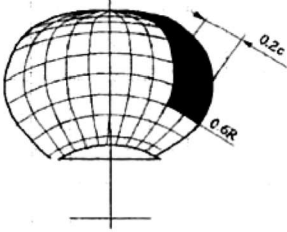
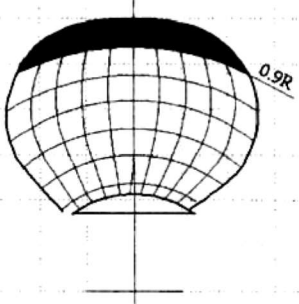
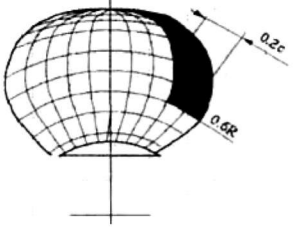
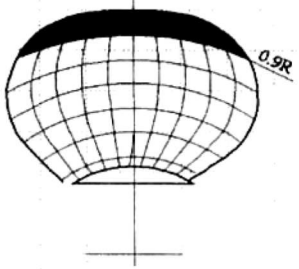
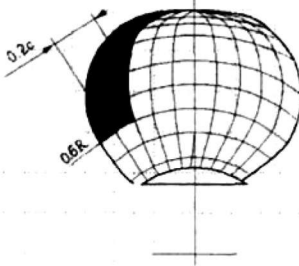
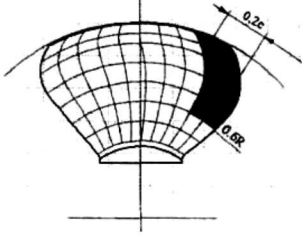
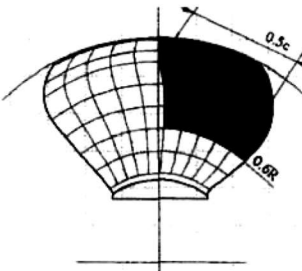
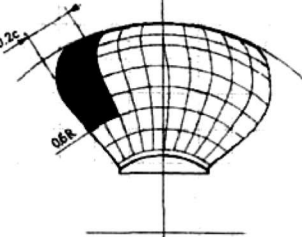
	Force	Loaded area	Right handed propeller blade seen from back
Load case 1	F_b	Uniform pressure applied on the back of the blade (suction side) to an area from $0,6R$ to the tip and from the leading edge to $0,2$ times the chord length	
Load case 2	50 per cent of F_b	Uniform pressure applied on the back of the blade (suction side) on the propeller tip area outside of $0,9R$	
Load case 3	F_f	Uniform pressure applied on the blade face (pressure side) to an area from $0,6R$ to the tip and from the leading edge to $0,2$ times the chord length	
Load case 4	50 per cent of F_f	Uniform pressure applied on propeller face (pressure side) on the propeller tip area outside of $0,9R$	
Load case 5	60 per cent of F_f or F_b which one is greater	Uniform pressure applied on propeller face (pressure side) to an area from $0,6R$ to the tip and from the trailing edge to $0,2$ times the chord length	

Table 2

Load cases for ducted propeller			
	Force	Loaded area	Right handed propeller blade seen from back
Load case 1	F_b	Uniform pressure applied on the back of the blade (suction side) to an area from $0,6R$ to the tip and from the leading edge to $0,2$ times the chord length	
Load case 3	F_f	Uniform pressure applied on the blade face (pressure side) to an area from $0,6R$ to the tip and from the leading edge to $0,5$ times the chord length	
Load case 5	60 per cent of F_f or F_b which one is greater	Uniform pressure applied on propeller face (pressure side) to an area from $0,6R$ to the tip and from the trailing edge to $0,2$ times the chord length	

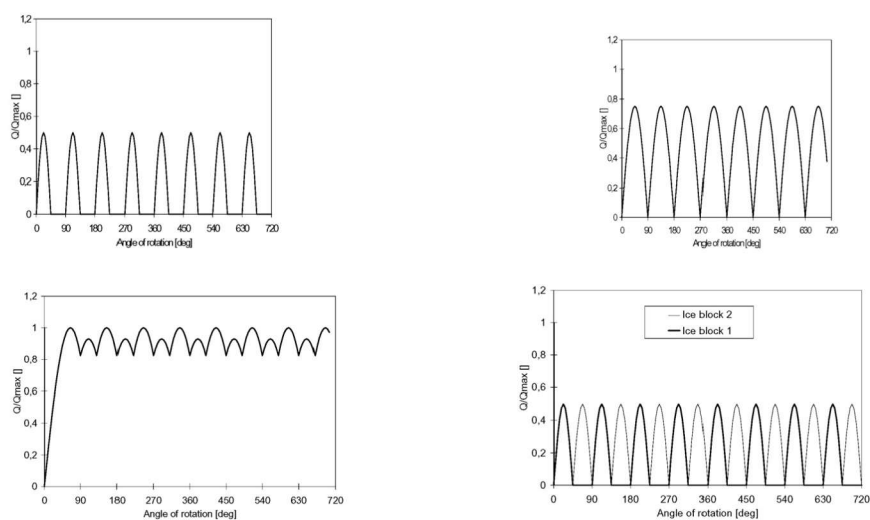


Fig. 1

The shape of the propeller ice torque excitation for 45, 90, 135 degrees single blade impact sequences and 45 degrees double blade impact sequence (two ice pieces) on a four bladed propeller

2 TECHNICAL REQUIREMENTS FOR ESCORT TUGS

2.1 GENERAL

2.1.1 Scope of application.

2.1.1.1 The technical requirements for escort tugs apply to tugs intended for escort service. These requirements are additional to the requirements of Parts I to XV of the Rules.

2.1.1.2 Tugs complying with the requirements of the present Section may be assigned the descriptive notation **Escort tug** added to the character of classification.

2.1.2 Definitions and explanations.

For the purpose of the present Section the following definitions and explanations have been adopted.

Manoeuvring time means a minimum manoeuvring time, in s, from maintained oblique position of the tug (from the centerline of the assisted ship) giving the maximum transverse steering force on one side of the assisted ship to mirror position on the other side.

Maximum steering pull of the tug means the maximum transverse steering force, in t, exerted by the tug on the stern of the assisted ship at the escort test speed of 8 and/or 10 knots.

Escort test speed means the speed, in knots, of the assisted ship during full scale trials.

Assisted ship means the ship being escorted by the escort tug.

Full scale trials mean sea trials of the escort tug to determine escort characteristics.

Escort service means steering, braking and otherwise controlling the assisted ship.

Escort characteristics:

maximum steering pull of the tug F_s , in t, at the escort test speed V , in knots, (refer to Fig. 2.1.2);

manoeuvring time t , in s.

Escort tug means a tug which in addition to towing and ship handling operations is intended for escort services.

2.1.3 Technical documentation.

2.1.3.1 Technical documentation to be submitted to the Register for approval shall include the following:

.1 towing arrangement plan required for escort service including towing line path and minimum breaking strength of towing line components and strength of appropriate structures;

.2 preliminary calculation of maximum steering pull of the tug at the escort test speed of 8 and/or 10 knots including propulsion components of the escort tug for balancing of oblique angular position of the tug;

.3 preliminary tug stability calculations for escorting service;

.4 plan of full scale trials.

2.2 TECHNICAL REQUIREMENTS

2.2.1 Arrangement and design.

2.2.1.1 A bulwark shall be fitted all around the exposed weather deck.

2.2.1.2 The towing winch intended for escort service shall be fitted with a load reducing system in order to prevent overload caused by dynamic oscillation in the towing line, and shall be capable of paying out the towing line if the pull exceeds 50 per cent of the breaking strength of the towing line.

2.2.1.3 The towing line components shall have a minimum breaking strength of at least 2,2 times the maximum towing pull as measured during the full scale trials (refer to 2.3).

2.2.1.4 In case of escort service of oil tankers and/or oil recovery vessels, supply vessels, ships intended for the carriage of explosives and inflammable cargoes, the requirements of 11.1.3, Part VIII "Systems and Piping" shall be complied with.

2.2.2 Stability.

2.2.2.1 In addition to the requirements for tugs set forth in 3.7, Part IV "Stability", stability of the escort tug shall comply with the criteria specified in 2.2.2.1.1 to 2.2.2.1.5.

2.2.2.1.1 The ratio between the righting and heeling areas between equilibrium and 20° angle of heel obtained

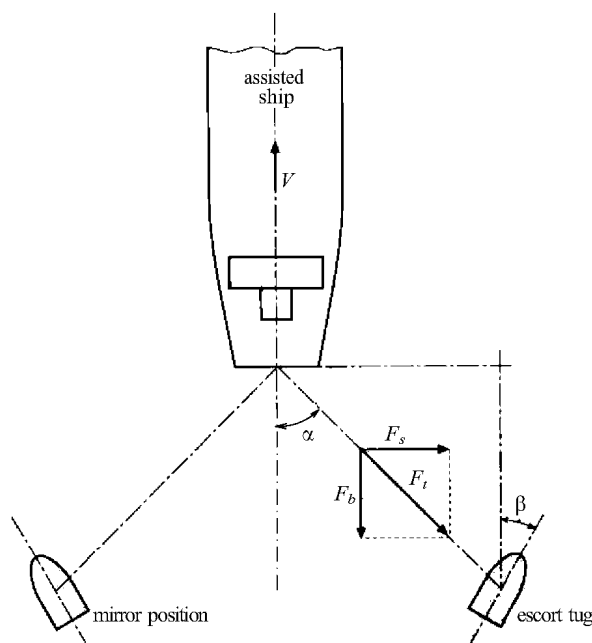


Fig. 2.1.2 Typical working mode of the escort tug
 F_s = steering pull; F_b = braking force; F_t = towing line tension;
 α = towing line angle; β = oblique angle;
 V = speed of the assisted ship

when the maximum steering pull F_s is applied from the tug (refer to Fig. 2.1.2) shall be not less than 1,25.

2.2.2.1.2 The ratio between the righting area and the heeling area due to the maximum steering pull between 0° heel and the angle of flooding or 40° angle of heel, whichever is less, shall be not less than 1,4.

2.2.2.1.3 The angle of heel of the escort tug under the effect of maximum working heeling moment, due to the towing line jerk under rolling shall not exceed the angle corresponding to the maximum of the righting lever curve θ_{\max} or the angle of flooding θ_f , whichever is less.

The following requirement shall be complied with (refer to Fig. 2.2.2.1.3):

$$K_3 = \sqrt{\frac{b+c}{a+c}} \geq 1,0 \quad (2.2.2.1.3-1)$$

where a = the area formed by the righting lever curve, the straight line corresponding to the lever $l + l_h$, and the angle of heel $\theta_1 - \theta_{2r}$;

b = the area formed from above by the righting lever curve, from below — by the straight line corresponding to the lever $l + l_h$, and from the right — by the angle corresponding to the maximum of the righting lever curve θ_{\max} or the angle of flooding θ_f , whichever is less;

c = the area formed from the left by the righting lever curve, from above — by the straight line corresponding to the lever $l + l_h$, from the right — by the angle corresponding to the maximum of the righting lever curve θ_{\max} or the angle of flooding θ_f , whichever is less.

When determining the angle of flooding θ_f , the definition of the angle of flooding given in 1.2, Part IV "Stability" shall be considered.

The heeling lever l_h characterizing the effect of towing line jerk, in m, is determined by the formula

$$l_h = 0,2 \left(1 + 2 \frac{d}{B} \right) \frac{b^2}{(1+c^2)(1+c^2+b^2)} \frac{57,3}{(\theta_{2r} - \theta_1 + \theta_{\lim})} \quad (2.2.2.1.3-2)$$

where d, B = the draft and breadth of the tug respectively;

c, b are calculated in accordance with 3.7.2.2, Part IV "Stability";
 $\theta_{\lim} = \theta_{\max}$ or θ_f , whichever is less.

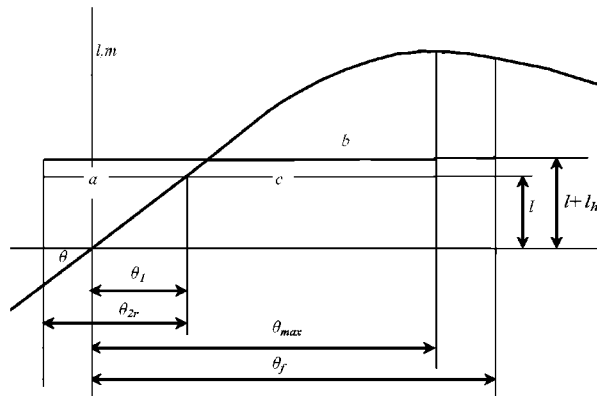


Fig. 2.2.2.1.3

2.2.2.1.4 The angle of dynamic heel of the tug which may occur during escort service in case of sudden failure of the main propulsion plant shall not exceed the angle corresponding to the maximum of the righting lever curve θ_{\max} or the angle of flooding θ_f , whichever is less.

2.2.2.1.5 At the design stage, the value of the maximum steering pull and the angle of heel under its effect may be determined based on the model tests results or by means of calculations. On completion of the ship's construction, the values of the maximum steering pull and the maximum possible angle of heel of the tug shall be ascertained based on the results of full scale trials.

2.3 FULL SCALE TRIALS

2.3.1 Plan of full scale trials.

2.3.1.1 Prior to the full scale trials the plan of the trials, the approved Information on Stability, as well as preliminary calculations of the ship's escort characteristics and the tug's stability during escort service shall be submitted to surveyor to the Register.

2.3.1.2 The plan of full scale trials shall stipulate determination of the tug's maximum transverse steering force at the speed of the assisted ship of 8 and/or 10 knots, the maximum angle of static heel at the specified modes, as well as the tug's manoeuvring time (refer to Fig. 2.1.2).

2.3.1.3 The plan shall include a list of measuring instruments, description of mandatory manoeuvres, a towing arrangement scheme for expected escort modes, design loads of strong points of the tug, as well as data of the safe working load of the strong points of the assisted ship.

2.3.2 Procedure of trials.

2.3.2.1 Full scale trials shall be carried out on:

.1 the first ship out of the series of ships, then every fifth ship of the series (i.e. sixth, eleventh, etc.) provided their propulsion plant is identical;

.2 every ship of non-series construction.

2.3.2.2 The trials shall be carried out in favourable weather (recommended limitation of wind force is 10 m/s, sea state 2), with the operating load of the tug equal to 50 — 10 per cent of provisions. Current velocity in the area of the trials (if any) shall be measured both upstream and down stream.

2.3.2.3 Displacement of the assisted ship shall be sufficient to maintain the heading and speed with the help of the autopilot during the necessary tug manoeuvring.

2.3.2.4 The following data shall be recorded continuously in real time mode during trials for later analysis:

.1 position of the assisted ship in relation to the escort tug;

.2 towing line tension;

.3 escort test speed;

.4 angle of the tug heel during escort service;

.5 length and angle of the towing line from the centerline of the assisted ship;

.6 manoeuvring time from maintained oblique position of the tug on one side of the assisted ship to mirror position on the other side at the maximum tension value of towing line and the maximum towing line angle from the centerline of the assisted ship (but not more than 60°);

.7 angle of heel due to sudden loss of thrust.

2.4 REPORTING

2.4.1 Report in tabular form on the results of the tug's trials to determine the escort characteristics and including records of the parameters measured in real time mode shall be agreed with the surveyor to the Register attending the trials and be forwarded to the Register

Head Office for consideration. The Report shall contain calculation of the steering pull value taking into account the time of the tug's transfer to the mirror position. The Report shall be accompanied with the escort tug's stability calculation based on results of full scale trials.

2.4.2 Results of full scale trials are documented in the Act issued by surveyor to the Register.

2.4.3 Upon satisfactory results of full scale trials and consideration of stability calculation specified in 2.4.1, in the Classification Certificate issued for the tug the descriptive notation **Escort tug** is added to the character of classification, and in the column "Other characteristics" the following entry shall be made: "During escort service the maximum steering pull is equal to t, with the escort test speed 8 (or 10) knots and the minimum manoeuvring times". In case the measurements were taken at two values of escort test speed (8 and 10 knots), the data of both speeds shall be recorded.

3 REQUIREMENTS FOR THE EQUIPMENT OF SHIPS IN COMPLIANCE WITH THE DISTINGUISHING MARKS ECO AND ECO-S IN THE CLASS NOTATION

3.1 GENERAL

3.1.1 Scope of application.

The requirements for the equipment of ships in compliance with the distinguishing marks **ECO** and **ECO-S** in the class notation have been developed taking into account the following international instruments as amended:

- .1 Annexes I, II, IV, V, VI to MARPOL 73/78;
- .2 provisions of the International Convention on the Control of Harmful Anti-Fouling Systems on Ships, 2001;
- .3 provisions of the International Convention for the Control and Management of Ships' Ballast Water and Sediments, 2004;
- .4 Guidelines for the Control and Management of Ships' Ballast Water to Minimize the Transfer of Harmful Aquatic Organisms and Pathogens (IMO resolution A.868(20));
- .5 Guidelines for On-Board Exhaust GAS-SO_x Cleaning System (IMO resolution MEPC.184(59));
- .6 Code on Intact Stability for All Types of Ships Covered by IMO Instruments (IMO resolution A.749(18));
- .7 provisions of IACS Unified Requirement L5 "Onboard computers for stability calculations" (Rev. 1, Feb. 2005);
- .8 IMO Guidelines on Ship Recycling, 2004 (IMO resolution A.962(23));
- .9 IMO Standards for Vapour Emission Control Systems (MSC/Circ.585);
- .10 provisions of Directive 99/32/EU with amendments to Directive 2005/33/EU;
- .11 provisions of the 1987 Montreal Protocol on Substances that Deplete the Ozone Layer;
- .12 Standard Specification for Shipboard Incinerators (IMO resolution MEPC.76(40));
- .13 revised Guidelines and Specifications for Pollution Prevention Equipment for Machinery Space Bilges of Ships (IMO resolution MEPC.107(49));
- .14 revised Guidelines and Specifications for Oil Discharge Monitoring and Control Systems for Oil Tankers (IMO resolution MEPC.108(49)).

The requirements of the present Section are applied during survey of ships for assigning the distinguishing marks **ECO** and **ECO-S** in the class notation (refer to 3.2.1).

3.1.2 Terms. Definitions.

Noxious liquid substance (NLS) means any substance indicated in the Pollution Category column of Chapters 17 and 18 of the International Bulk Chemical Code (IBC Code).

Emission to air means any emission to air from ships subject to control by Annex VI to MARPOL 73/78.

Segregated ballast means the ballast water introduced into a tank which is completely separated from the cargo oil and fuel oil system and which is permanently allocated to the carriage of ballast or to the carriage of ballast or cargoes other than oil or noxious liquid substances.

Bilge water means water accumulated in and subsequently removed from the ship's machinery spaces.

Garbage means garbage generated during normal operation of the ship, sorted, stored and disposed of/incinerated in accordance with the provisions of Annex V to MARPOL 73/78.

NLS tanker means a ship constructed or adapted to carry a cargo of noxious liquid substances in bulk and includes an "oil tanker" as defined in Annex I to MARPOL 73/78 when certified to carry a cargo or part cargo of noxious liquid substances.

Oil residues mean oil residues generated during normal operation of the ship and include the following:

- used lubricating and hydraulic oils;
- fuel oil and lubricating oil leaked from the ship's machinery and systems;
- sludge from fuel oil and lubricating oil separators, from bilge separators.

Oily mixture means a mixture with any oil content.

Cargo residues mean any noxious liquid substance or oily mixture that remain for subsequent disposal.

Passenger ship means a ship that carries more than 12 passengers. A passenger is every person other than the master and the members of the crew or other persons employed or engaged in any capacity on board a ship on the business of that ship, and a child under one year of age.

Anti-fouling systems mean coatings, paints, surface treatment and devices that are used on a ship to control or prevent attachment of unwanted organisms.

Fire-fighting systems mean shipboard fixed fire-fighting systems containing fire-fighting substances with different ozone depleting potential (ODP) and global warming potential (GWP) values.

SO_x Emission Control Areas mean areas where emission of sulphur oxides is limited as defined in Annex VI to MARPOL 73/78 and Directive 99/32/EU, as amended.

Regular service means a series of passenger ships voyages between the same two or more ports.

Discharge to sea means any discharge from ships to sea of harmful substances or effluents containing

such substances including any escape, disposal, spilling, leaking, pumping, emitting or emptying.

Bilge separator means any combination of a separator, filter or coalescer, and also a single unit designed to produce an effluent with oil content not exceeding 15 ppm or 5 ppm (whatever is applicable).

Bilge alarm means a device giving off a signal whenever the oil content in the effluent exceeds 15 ppm or 5 ppm (whatever is applicable).

Ballast water system means a system comprising tanks for ballast water and associated piping and pumping systems (combined cargo/ballast tanks are not considered in the present Section).

Sewage system means a system comprising the following equipment:

sewage holding tank; or
sewage holding tank and comminuter; or
sewage treatment plant;
discharge pipeline with pumps and standard discharge connections.

Sewage means sewage generated during normal operation of the ship and includes drainage as defined in Annex IV to MARPOL 73/78.

Ship at berth means a ship moored or anchored in port while loading, unloading or hosteling, including the time spent when not engaged in cargo operations.

Chemical tanker means a ship constructed or adapted for the carriage in bulk of any liquid product listed in Chapter 17 of the IBC Code.

Sanitary and domestic waste waters mean drainage from wash basins, showers, laundries, wash tubes and scuppers, drainage from sinks and equipment of galleys and spaces annexed to galleys.

Refrigeration systems means shipboard systems (cargo refrigeration plants, air conditioning and refrigeration systems) containing refrigerants with different ozone depleting potential (ODP) and global warming potential (GWP) values.

3.2 CLASSIFICATION

3.2.1 Application.

The requirements of the present Section apply to the equipment and systems for prevention of pollution from emissions to air and discharges to sea and are aimed at prevention of environmental pollution in case of emergency.

Ships complying with the requirements of the present Section may be assigned the following distinguishing marks in the class notation:

ECO — the distinguishing mark in the class notation, which identifies compliance with the basic requirements for controlling and limiting operational emissions and discharges as well as requirements for prevention of environmental pollution in case of emergency (the requirements are specified in 3.5);

ECO-S — the distinguishing mark in the class notation, which identifies compliance with more stringent requirements than those for assignment of the distinguishing mark **ECO** in the class notation (the requirements are specified in 3.6).

It is recommended to assign the above distinguishing marks in the class notation to the following ships:

ECO — to newbuildings and existing ships;

ECO-S — to newbuildings, existing passenger and coastal ships.

3.2.2 Requirements for ships with the distinguishing marks ECO and ECO-S in the class notation.

Requirements	Distinguishing marks in the class notation	
	ECO	ECO-S
The following requirements shall be met on ships regarding prevention of air pollution:		
3.5.2.2 Prevention of pollution by emission from marine diesel engines	×	×
3.6.2.2 Prevention of pollution by emission from marine diesel engines	—	×
3.5.2.3 Prevention of pollution by emission from boilers and inert gas generators	×	×
3.6.2.3 Prevention of pollution by emission from boilers and inert gas generators	—	×
3.5.2.4 Prevention of pollution by refrigerant emission	×	×
3.6.2.4 Prevention of pollution by refrigerant emission	—	×
3.5.2.5 Prevention of pollution by fire extinguishing media emission	×	×
3.6.2.5 Prevention of pollution by fire extinguishing media emission	—	×
3.5.2.6 and 3.6.2.6 Prevention of pollution by volatile organic compounds emission	×	×
3.5.2.7 and 3.6.2.7 Prevention of pollution by emissions from shipboard incinerators.	×	×
The following requirements shall be met on ships regarding prevention of pollution of the marine environment:		
3.5.3.2 Discharge of cargo residues.	×	×
3.6.3.2 Discharge of cargo residues.	—	×
3.5.3.3 Structural measures and equipment for prevention of oil spills during cargo operations and bunkering.	×	×
3.6.3.3 Structural measures and equipment for prevention of oil spills during cargo operations and bunkering.	—	×
3.5.3.4 and 3.6.3.4 Ballast water management.	×	×
3.5.3.5 Prevention of pollution at oil contaminated water discharge	×	×
3.6.3.5 Prevention of pollution at oil contaminated water discharge	—	×
3.5.3.6 Prevention of pollution by garbage	×	×
3.6.3.6 Prevention of pollution by garbage	—	×
3.5.3.7 Prevention of pollution by sewage	×	×
3.6.3.7 Prevention of pollution by sewage	—	×
3.5.3.8 and 3.6.3.8 Control of harmful anti-fouling systems	×	×
3.5.3.9 and 3.6.3.9 Prevention of lubricating oil and hydraulic oil leakages into seawater	×	×
3.5.3.10 Prevention of pollution in case of the hull damage	×	×

Requirements	Distinguishing marks in the class notation	
	ECO	ECO-S
3.6.3.10 Prevention of pollution in case of the hull damage	—	×
The following requirements shall be met on ships regarding prevention of pollution at ship recycling:		
3.5.4 and 3.6.5 Prevention of pollution at ship recycling	×	×

3.2.3 Any ship shall have **AUT1** or **AUT2** distinguishing automation mark of the machinery installation in the class notation.

3.2.4 Assignment of the distinguishing marks in the class notation to oil tankers of less than 150 gross tonnage, to other ships of less than 400 gross tonnage and to floating facilities for oil storage and production is subject to special consideration by the Register in each particular case.

3.3 APPLICATION OF INTERNATIONAL INSTRUMENTS' REQUIREMENTS

3.3.1 The requirements of the present Section are based on international instruments, the main of which are specified in 3.1. At the same time, some provisions of the requirements of the present Section are more stringent than the requirements of the relevant international instruments.

3.3.2 Required compliance of the ship's systems and equipment with international instruments.

Ship's systems and equipment	International instrument
15 ppm bilge separators	IMO resolution MEPC.107(49)
15 ppm bilge alarms	IMO resolution MEPC.107(49)
Oil discharge monitoring and control systems	IMO resolution MEPC.108(49)
Oil/water interface detectors	IMO resolution MEPC.5(XIII)
Shipboard incinerators	Regulation 16 of Annex VI to MARPOL 73/78, IMO resolution MEPC.76(40)
Sewage treatment plants	IMO resolution MEPC.2(VI), MEPC159(55)
Cargo vapour collection systems of oil tankers	Regulation 15 of Annex VI to MARPOL 73/78, MSC/CIRC.585
Marine diesel engines	Regulation 13 of Annex VI to MARPOL 73/78, NO _x Technical Code
Exhaust gas cleaning systems to reduce the emission of sulphur oxides (SO _x)	Regulation 14 of Annex VI to MARPOL 73/78, IMO resolution MEPC.184(59)

3.3.3 International regulations and standards for use of fuel oil on ships, bunkering, sampling and testing of fuel oil.

Required processes, specifications	International instrument
Sampling of fuel oil	IMO resolution MEPC.182(59), GOST 2517-85
Standard marine fuel oil	ISO 8217
Bunkering of ships	Regulation 18 of Annex VI to MARPOL 73/78
Fuel oil sulphur content test	ISO 8754

3.4 REQUIRED DOCUMENTATION

3.4.1 Technical documentation and certificates required for assigning the distinguishing marks **ECO** and **ECO-S** in the class notation:

.1 International Air Pollution Prevention (IAPP) Certificate;

.2 Engine International Air Pollution Prevention (EIAPP) Certificate;

.3 Approved Technical File of the engine on the NO_x emission for each engine subject to survey in accordance with the NO_x Technical Code;

.4 SO_x Emission Control Area Compliance Certificate (SCC);

.5 Exhaust Gas Cleaning System — SO_x Technical Manual (ETM);

.6 International Sewage Pollution Prevention Certificate;

.7 Certificate of Compliance of Equipment and Arrangements of the Ship with the Requirements of Annex V to MARPOL 73/78;

.8 International Anti-Fouling System Certificate/Statement of Compliance of Anti-Fouling System or Declaration on Anti-Fouling System in Compliance with International Convention on the Control of Harmful Anti-Fouling Systems on Ships, 2001 (refer to 3.5.3.8);

.9 approved documentation confirming compliance of the oil tanker with the requirements for double hull construction in accordance with regulation 19 of Annex I to MARPOL 73/78;

.10 approved documentation confirming compliance of the ship with the requirements for protective location of fuel oil tanks as defined in regulation 12A of Annex I to MARPOL 73/78 (refer to 3.5.3.10.5 to 3.5.3.10.7 and 3.6.3.10.2);

.11 approved documentation on the ship's fuel oil system confirming possibility of ready change over to low-sulphur content fuel oil when approaching SO_x emission control areas established under Annex VI to MARPOL 73/78 or Directive 99/32/EU accordingly;

.12 Statement of Compliance to IMO resolution on Ship Recycling "Green Passport".

3.4.2 Approved operating procedures for assigning the distinguishing marks **ECO** and **ECO-S** in the class notation:

.1 approved On-Board Monitoring Manual (OMM);
.2 approved SO_x Emission Compliance Plan (SECP);
.3 procedure for preparing the ship's fuel oil system for operation in the SO_x emission control area (SECA);
.4 approved Fuel Oil Management Plan, Fuel Oil Record Book;

.5 approved ship's Ballast Water Management Plan (in case of ballast water exchange at sea - approved special software for ballast exchange at sea) and approved Ballast Water Record Book;

.6 approved ship's software for calculation of intact trim, stability and strength as well as damage trim and stability;

.7 approved ship's software for planning the ballast water exchange at sea (if applicable in accordance with 3.5.3.4.2);

.8 approved Shipboard Oil Pollution Emergency Plan or Shipboard Marine Pollution Emergency Plan (for Oil and Noxious Liquid Substances) keeping due note of regulation 37.4, Annex I to MARPOL 73/78 in relation to fast access to computerized shore-based software for calculation of damage stability and residual structural strength, as well as Oil Record Book, parts I and II (regulations 17 and 36 of Annex I to MARPOL 73/78);

.9 approved Shipboard Marine Pollution Emergency Plan for Noxious Liquid Substances (regulation 17 of Annex II to MARPOL 73/78), approved Procedures and Arrangement Manual (regulation 14 of Annex II to MARPOL 73/78) and Cargo Record Book (regulation 15 of Annex II to MARPOL 73/78);

.10 refrigerating operations management procedure;

.11 approved Sewage Management Plan; Sewage Record Book;

.12 Record Book of Detection of Lubricating Oil and Hydraulic Oil Operating Leakages onto Seawater Surface;

.13 Volatile Organic Compound (VOC) Management Plan;

.14 Transfer of oil cargo between oil tankers at sea (STS operations) Plan.

3.4.3 Ship's technical documentation for assigning the distinguishing marks **ECO** and **ECO-S** in the class notation:

.1 ship's general arrangement plan and tanks plan;

.2 fuel oil system diagram including drawings of arrangements and systems enabling transition of machinery operation on low-sulphur content fuel oil, if applicable;

.3 drawings of any exhaust gas cleaning systems, which shall be approved in accordance with the IMO Guidelines;

.4 refrigerating systems diagrams, list of refrigerants used;

.5 fire-fighting systems diagrams, list of fire extinguishing media used in these systems;

.6 incinerator systems diagrams;

.7 diagrams of manifolds in cargo and non-cargo areas including trays and appliances for prevention of oil spill;

.8 diagrams and drawings of fuel oil system, bilge system, oil discharge, monitoring and control system for ballast and flushing water, ballast water system;

.9 diagrams and drawings of the equipment for the prevention of pollution by garbage;

.10 sewage system diagram.

3.5 TECHNICAL REQUIREMENTS FOR ASSIGNING THE DISTINGUISHING MARK ECO IN THE CLASS NOTATION

3.5.1 Introduction.

3.5.1.1 The provisions of the present Chapter cover the requirements on emissions to air from sources of power, oil tanker cargo systems and service systems onboard, as well as requirements for discharges to sea from sources of power, from ship's systems and equipment of machinery spaces and from cargo areas of oil tankers, chemical tankers and NLS tankers, from sewage systems, anti-fouling and ballast systems, as well as the requirements for the prevention of pollution by garbage.

3.5.1.2 The required documentation is specified in 3.4.

3.5.2 Prevention of air pollution.

3.5.2.1 General.

3.5.2.1.1 Fuel oil supplied to the ship shall not contain inorganic acids or chemical wastes that can endanger a ship, bring harm to the crew or that can add to air pollution.

3.5.2.1.2 Fuel oil shall be controlled in accordance with Fuel Oil Management Plan, Fuel Oil Record Book.

Quality of ordered fuel oil and quality of received fuel oil according to bunker delivery note shall be documented in Fuel Oil Record Book (refer to regulations 18.3 and 18.4 of Annex VI to MARPOL 73/78, as well as Directive 99/32/EU, as amended).

Fuel Oil Management Plan shall comprise adequate procedures for replacement of fuel oil in order to make sure that fuel oil burnt in the engine in the SO_x emission control area is of the required quality. Relevant ship's log shall contain evidence that the fuel oil of the required quality was used in relevant areas.

3.5.2.1.3 SECP shall be readily available in all ships using exhaust gas cleaning system to reduce SO_x emission to confirm compliance with the requirements of regulations 14.1 and 4.14 of Annex VI to MARPOL 73/78.

This Plan shall list all ship's plants for burning fuel oil, which comply with the operating requirements specified in the above regulations by adoption of the approved system specified above.

3.5.2.1.4 Bunker delivery note shall be accompanied by sample of supplied fuel oil properly sealed and signed

by representatives of the bunkering company, ship master or ship officer responsible for bunkering operations. Bunker delivery note shall be kept onboard for three years. Fuel oil sample shall be stored under ship's officers control until the end of consumption but not less than 12 months from the date of supply.

This note shall confirm that a fuel oil is supplied in accordance with regulations 14 and 18 of Annex VI to MARPOL 73/78, i.e. sulphur content in the supplied fuel oil complies with the applicable requirements and there are no inorganic acids and chemical wastes in this fuel oil.

For the purpose of cross-reference the number of sample shall be stated in the note.

3.5.2.1.5 Sampling equipment and testing procedures shall comply with provisions of documents specified in 3.3.3.

In order to fulfill the requirements of IMO resolution MEPC.182(59) in respect of method and place of fuel oil sampling the ship shall be fitted with the sampling device of approved structure (irrespective whether the fuel oil supplier has a sampling device for installation on the inlet header of receiving ship or not).

3.5.2.1.6 The ship shall have a valid International Air Pollution Prevention (IAPP) Certificate in accordance with Annex VI to MARPOL 73/78.

3.5.2.2 Prevention of pollution by emission from marine diesel engines.

3.5.2.2.1 NO_x emission restrictions are applied to engines permanently fitted onboard of power more than 130 kW except engines that are part of any equipment used in emergency solely and engines on lifeboats.

3.5.2.2.2 Level of emission from engines on all ships shall comply with Annex VI to MARPOL 73/78.

3.5.2.2.3 If NO_x emission is monitored on ships by means of devices fitted in fuel oil or exhaust gas systems or in addition to them, then such systems shall be operated and controlled in accordance with procedures including manufacturers' manuals and shall be approved by the Register or other classification society.

3.5.2.2.4 Appropriate international certificates shall be issued to marine engines of power more than 130 kW (except emergency ones and those for lifeboats) and to exhaust gas cleaning systems to reduce SO_x emission (if applicable) in accordance with Annex VI to MARPOL 73/78 and IMO resolution MEPC.184(59).

3.5.2.2.5 If the exhaust gas cleaning system is used to reduce NO_x emission, the engine and the above system for which it is installed are treated as a single whole. The exhaust gas cleaning system to reduce NO_x emission shall be of approved design.

3.5.2.2.6 Measurements of NO_x emission level from diesel engines with exhaust gas cleaning system to reduce NO_x emission or without it shall comply with methods specified in the NO_x Technical Code. Measurements and tests shall be performed and documented in

accordance with the provisions of the Guidelines on Marine Diesel Engines Survey in Compliance with the Technical Code on Control of Emission of Nitrogen Oxides from Marine Diesel Engines.

3.5.2.2.7 Compliance with SO_x emission restrictions is mainly achieved by use of low-sulphur content fuel oil. Alternatively, an exhaust gas cleaning system may be used to reduce SO_x emission to attain the required level of SO_x emission. The maximum sulphur content in fuel oil supplied to the ship is 3,5 per cent. When an exhaust gas cleaning system is used, the SO₂ (ppm)/CO₂ (% v/v) ratio shall not exceed 151,7.

3.5.2.2.8 If a ship operates in SO_x emission control area (including ports) the sulphur content in fuel oil shall not exceed 1,00 per cent. When an exhaust gas cleaning system is used, the SO₂ (ppm)/CO₂ (% v/v) ratio shall not exceed 43,3.

3.5.2.2.9 During operation of ships in the territorial seas, coastal zones and EU ports the sulphur content in fuel oil shall not exceed values specified in EU Council Directive 1999/32/EU, as amended (articles 3 and 4).

3.5.2.2.10 During operation of passenger ships engaged on the regular voyages to/from the EU ports the sulphur content in fuel oil shall not exceed values specified in Directive 2005/33/EU (article 4a).

3.5.2.2.11 Transition from one type of fuel oil to another while coming in and out of the SO_x emission control areas specified in Annex VI to MARPOL 73/78, as well as while coming in and out of the EU territorial waters including mooring and anchoring in the EU ports shall be registered in the ship's log.

3.5.2.2.12 During survey of engines fitted with the exhaust gas cleaning systems to reduce SO_x emission, the compliance with SO_x emission norms specified in the Guidelines for On-Board Exhaust GAS-SO_x Cleaning System (IMO resolution MEPC.184(59)) shall be confirmed.

3.5.2.3 Prevention of pollution by emission from boilers and inert gas generators.

3.5.2.3.1 Compliance with restrictions of SO_x emission from boilers and inert gas generators is mainly achieved by use of low-sulphur content fuel oil with sulphur content complying with 3.5.2.2.7 to 3.5.2.2.10.

3.5.2.3.2 Alternatively, an exhaust gas cleaning system may be used to reduce SO_x emission to reach the required level of SO_x emission. The use of such system is subject to special consideration by the Register in each particular case.

3.5.2.4 Prevention of pollution by refrigerant emission.

3.5.2.4.1 The requirements of the present Section for prevention of pollution by refrigerant emission are applied to cargo refrigerating plants, air conditioning plants and refrigerating systems of all ships.

The said requirements are not applied to autonomous home air-conditioners, refrigerators and freezers perma-

nently sealed and having no connections for refrigerant charging onboard.

3.5.2.4.2 In accordance with provisions of the Montreal Protocol 1987 criteria for refrigerant emission are limited by requirements relative to qualities of used refrigerants in relation to their ozone depleting potential (ODP) and global warming potential (GWP).

3.5.2.4.3 It is not allowed to use ozone-depleting substances on ships.

The following substances may be used as refrigerants onboard:

natural refrigerants (such as, ammonia (NH₃) or carbonic acid (CO₂));

hydro fluorocarbon (HFC) with ODP = 0 and GWP < 3500.

3.5.2.4.4 The Refrigerant Management Procedure shall be implemented on board the ships to control presence of leaks which shall contain as a minimum the following issues:

operation of refrigerating plants to prevent/minimize possible leaks;

periodicity of inspections of refrigerating plants aimed at finding leaks and keeping records of their quantity;

performing corrective actions if leaks exceed norms, operating limitations to prevent such leaks.

Corrective actions shall be performed before the quantity of leaks reaches 10 per cent of the total quantity of refrigerant in each system.

3.5.2.4.5 In order to regenerate a refrigerant, compressors shall be able to discharge refrigerant from the system into the relevant receiver of the liquid refrigerant. Additionally, regenerating units shall be fitted to discharge refrigerant from the system into the existing refrigerant receivers or appropriate receivers.

3.5.2.4.6 When different types of refrigerants are used, measures shall be provided to prevent mixing of such substances.

3.5.2.4.7 In order to make sure there are no emissions to air or that they are reduced to minimum, refrigerants in the refrigerating systems shall be controlled by appropriate method to discover all types of leaks, including those that are usually not discovered by the automatic leak detection system.

One of the following methods or combination thereof may be used:

leak detection system appropriate for the used refrigerant with signaling if refrigerant is found outside refrigerating system;

measuring of refrigerant level in the refrigerating system with low level signaling;

registering refrigerant level in special journal at certain intervals (once in a week as a minimum) to find out minor leaks.

3.5.2.5 Prevention of pollution by fire extinguishing media emission.

3.5.2.5.1 Natural fire extinguishing media (such as argon, nitrogen, CO₂) used in fixed fire extinguishing systems are not considered as ozone depleting substances.

3.5.2.5.2 When other fire extinguishing media (for instance, hydrofluorocarbons (HFC) are used in fixed fire extinguishing systems, the media shall have the following properties: GWP < 4000, ODP = 0.

3.5.2.6 Prevention of pollution by volatile organic compounds emission.

3.5.2.6.1 In order to prevent emission of VOC from oil tankers carrying crude oil, petroleum products, as well as from chemical tankers carrying chemical cargoes with flashpoint < 60°C, standards for cargo vapour discharge systems shall be applied according to MSC/Circ.585.

3.5.2.6.2 Approved technical documentation for the cargo vapour discharge system including principal diagram of the pipeline for vapour collection on oil tanker with indication of location and purpose of all control and safety arrangements as well as cargo transfer instruction shall be available onboard. This instruction shall contain information on the maximum permissible speed of cargo transfer, maximum pressure drop in the ship vapour collection system at different speeds of loading, operation threshold of each high-speed or vacuum valve etc.

3.5.2.6.3 In addition to the International Air Pollution Prevention (IAPP) Certificate there shall be a note on the presence of cargo vapour collection system fitted and approved in accordance with MSC/Circ.585.

3.5.2.6.4 An approved VOC Management Plan shall be available on board the ship.

3.5.2.7 Prevention of pollution by emission from shipboard incinerators.

3.5.2.7.1 Shipboard incinerators shall be type-approved in accordance with IMO resolution MEPC.76(40).

3.5.2.7.2 Approved diagrams of the incinerator systems, the copy of Incinerator Type Approval Certificate as well as incinerator operational manual shall be available on board the ship.

3.5.2.7.3 The Certificate of Compliance of Equipment and Arrangements of the Ship with the Requirements of Annex V to MARPOL 73/78, as well as the Appendix to the International Air Pollution Prevention (IAPP) Certificate shall contain notes on shipboard incinerator corresponding to IMO resolution MEPC.76(40).

3.5.2.7.4 Operation of incinerators shall be in accordance with regulation 16 of Annex VI to MARPOL 73/78 and the approved Garbage Management Plan, and be recorded in the Garbage Record Book specified in regulations 9(2) and 9(3) of Annex V to MARPOL 73/78, respectively.

3.5.3 Prevention of marine environment pollution.

3.5.3.1 General.

Compliance with the requirements shall be confirmed in accordance with 3.2 to 3.4.

3.5.3.2 Discharge of cargo residues.

3.5.3.2.1 Discharge criteria for cargo residues apply to tankers carrying crude oil, petroleum products or noxious substances in bulk.

3.5.3.2.2 Discharge of contaminated ballast water or washing water from the area of cargo tanks of oil tankers, as well as discharge of bilge water from machinery spaces of any ship shall be carried out by the system of automatic measuring, record and control of discharge of ballast and washing water, as well as filtering equipment for discharge of bilge water, respectively. Discharge criteria shall be in compliance with Annex I to MARPOL 73/78.

3.5.3.2.3 Each tanker designed for the carriage of noxious substances in bulk shall be equipped with pumps and pipelines, providing stripping of each tank carrying cargoes with pollution categories X, Y and Z, in the way that the quantity of residues in the tank and associated piping does not exceed 75 l in accordance with Annex II to MARPOL 73/78. Discharge of contaminated water to sea shall be carried out by means specified in Annex II to MARPOL 73/78.

3.5.3.2.4 The above discharges and discharge to shore reception facilities shall be documented in the Oil Record Book, or Cargo Record Book, for oil tankers and chemical tankers, respectively.

3.5.3.3 Structural measures and equipment for prevention of oil spills during cargo operations and bunkering.

3.5.3.3.1 Oil tankers, chemical tankers and NLS tankers shall have fitted and implemented means and arrangements to reduce the possibility of oil or NLS spill on deck reaching the sea.

3.5.3.3.2 To keep cargo spills within the cargo area, provision shall be made for a permanent continuous coaming on the cargo deck extending from side to side and from a point 0,2L forward of amidships to the aft end of the cargo deck with the minimum heights given in Table 3.5.3.3.2:

Table 3.5.3.3.2

Minimum heights of continuous coaming		
Ships of 100000 t deadweight and over	0,2L forward of amidships	0,25 m
	Aft end of cargo deck	0,40 m
Ships of less than 100000 t deadweight	0,2L forward of amidships	0,10 m
	Aft end of cargo deck	0,25 m

3.5.3.3.3 To collect possible oil spills during cargo operations the main deck in the cargo area shall be fitted with a deck scupper system for collection of the spilled cargo with its accumulation in the holding tank or a slop tank. The deck scupper system may be arranged either with a manually operated valve or with automatic scuppers.

The drainage shall be used during cargo operations where cargo spills may occur, and shall not be used under normal conditions when at sea. When at sea, deck scupper system shall preclude free surface effect with negative impact on the ship's stability.

3.5.3.3.4 On oil tankers, chemical tankers and NLS tankers the points where cargo hoses are connected to cargo manifolds shall be fitted with spill trays with arrangement for spills collection to the tank.

The trays shall have the following minimum dimensions:

tray length shall be so that the cargo manifold doesn't extend beyond forward and aft ends of the tray;

width — at least 1,8 m, at that the spill tray extends at least 1,2 m outboard of the end of the manifold flange;

minimum depth — 0,3 m.

3.5.3.3.5 Oil tankers, chemical tankers and NLS tankers shall be fitted with means to adequately support hoses in way of ship's side abreast of manifolds. The support shall preferably be arranged as a horizontal curved plate or pipe section.

3.5.3.3.6 Oil tankers, chemical tankers and NLS tankers shall be fitted with a closed sounding system with high and maximum level alarms. Alternatively, a high level alarm may be accepted in combination with a closed sounding system, provided the alarm is independent from the sounding system.

3.5.3.3.7 Fuel oil, lubricating oil and other petroleum products bunker tanks on all ships shall be fitted with high level alarm to prevent overfilling.

3.5.3.3.8 Bunkering stations, vent and overflow pipes and other areas where petroleum products spills may occur shall be fitted with spill trays to prevent their escape to sea. Capacity: 80 l for ships of 300 to 1600 gross tonnage; 160 l for ships of 1600 gross tonnage and above.

3.5.3.3.9 Any oil tanker involved in STS operations shall carry on board an approved plan how to conduct STS operations (STS operations Plan) in compliance with IMO resolution MEPC.186(59).

3.5.3.4 Ballast water management.

3.5.3.4.1 Ballast water management is aimed at minimizing or prevention of transport of harmful aquatic organisms and pathogens from one geographical area to another. For this purpose, the special means for ship's ballast water management specified in regulation B-3 of the International Convention for the Control and Management of Ship's Ballast Water and Sediments, 2004, shall be provided onboard.

3.5.3.4.2 All ships where the method of ballast water exchange at sea is used for ballast water management, shall be provided with the Ballast Water Management Plan according to the Instruction for the Development of Ballast Water Management Plans developed for each ship and approved by the Register.

If the planning of ballast water exchange by the crew is provided for, the ship shall be additionally provided with special software programs for ballast water exchange planning.

3.5.3.4.3 Ballast system used during ballast water exchange at sea shall comply with the requirements of 8.7, Part VIII "Systems and Piping".

3.5.3.4.4 Any ship shall carry on board an approved Ballast Water Management Plan and Ballast Water Record Book.

3.5.3.4.5 Any ship fitted with ballast water treatment system shall have a copy of the Type Approval Certificate for this system issued by the Register on behalf of the Administration of the Russian Federation.

3.5.3.5 Prevention of pollution at oil contaminated water discharge.

3.5.3.5.1 Oil contaminated water discharge requirements apply to all ships according to regulations 15 and 34 of Annex I to MARPOL 73/78.

3.5.3.5.2 In addition to the requirements of Annex I to MARPOL 73/78, each ship shall be fitted with the bilge water holding tank of sufficient capacity agreed with the Register for bilge water disposal to reception facilities.

3.5.3.6 Prevention of pollution by garbage.

3.5.3.6.1 Requirements for availability of placards, Garbage Management Plan and garbage record keeping apply to all ships according to regulation 9 of Annex V to MARPOL 73/78.

3.5.3.6.2 A procedure for garbage sorting and volume reducing shall be available onboard in addition to Garbage Management Plan.

3.5.3.6.3 A ship shall be equipped with the marked containers with tight covers for garbage sorting, collection and storage prior to its discharge to the sea in the allowed areas in accordance with the regulations 3 to 5 of Annex V to MARPOL 73/78 or prior to its incineration in the ship incinerators or discharge to shore reception facilities.

3.5.3.7 Prevention of pollution by sewage.

3.5.3.7.1 All ships shall have a valid International Sewage Pollution Prevention Certificate.

3.5.3.7.2 All ships shall as a minimum be fitted with a sewage comminution and disinfection system approved by the ship's officers, and a sewage holding tank of sufficient capacity with visual and audible alarm operating in case of 80 per cent filling of the tank.

3.5.3.7.3 All ships shall be fitted with pipelines with a standard discharge connection in accordance with regulation 10 of Annex IV to MARPOL 73/78 for sewage discharge to reception facilities.

3.5.3.7.4 All ships shall be provided with calculations of the rate of discharge of untreated sewage approved by the Register. These calculations shall be drawn up according to Recommendation on Standards for the Rate of Discharge of Untreated Sewage from Ships (refer to IMO resolution MEPC.157(55)).

Where a ship shall discharge sewage from a holding tank using a pump with a fixed delivery, the pump can either be calibrated at the rate permitted at 4 knots, or calibrated for a specific minimum ship's speed in excess of 4 knots.

In case of pump with a variable delivery the rate of discharge may be increased up to maximum permissible discharge rate which corresponds to the ship's maximum summer draught and maximum service speed by

increasing of pump delivery provided the ship's speed corresponds to the maximum rate of discharge.

3.5.3.7.5 All sewage discharges, whether to sea or to shore-based reception facilities shall be recorded in the appropriate record book with indication of date, location and quantity of sewage discharged. In cases where untreated sewage is discharged to sea, the record shall include information on the ship's speed which shall correspond to the approved rate of discharge and the distance to the nearest shore (more 12 nautical miles¹) at the moment of discharge.

3.5.3.8 Anti-fouling systems

3.5.3.8.1 Anti-fouling systems (coatings) containing organo-tin compounds (Tributyltin (TBT)) as the active ingredients are not permitted.

3.5.3.8.2 Ships of 400 gross tonnage and upwards shall carry International Anti-Fouling System Certificate/Statement of Compliance of Anti-Fouling System with the International Convention on the Control of Harmful Anti-Fouling Systems on Ships, 2001 (AFS-Convention).

3.5.3.8.3 Ships having a length of 24 m (IC66) and more but of less than 400 gross tonnage shall carry declarations on compliance of their anti-fouling systems with AFS-Convention in accordance with form of Addenda 2 to Annex 4 to AFS Convention or with Annex III of EU Regulation 782/2003 (Regulation 5 of Annex 4 to AFS-Convention).

3.5.3.9 Prevention of lubricating oil and hydraulic oil leakages into seawater.

3.5.3.9.1 Requirements for prevention of leakages of lubricating oil and hydraulic oil into seawater shall be applied in the following cases:

if oil-lubricated stern tube bearings and sealing arrangements are provided;

if there is a possibility that lubricating oil will spill into the seawater from the lubricating oil system of the steering gear bearing;

if seawater cooled engines are provided;

if there is a probability that oil from the hydraulic system will spill into the seawater.

3.5.3.9.2 Occurrence of lubricating oil and hydraulic oil operating leakages into seawater shall be continuously monitored. If evidence of leakage is found, corrective actions shall be initiated and recorded in the ship's log. For this purpose all the insignificant oil leaks shall be monitored by the approved manual or automatic methods.

3.5.3.9.3 In case of oil-lubricated stern tube bearings and/or sealing arrangements, the above requirements shall be considered in addition to the requirements for oil level indicators and low level alarm of lubricating oil tanks as well as environmental safety of stern tube arrangements (refer to 5.6.4 and 5.7, Part VII "Machinery Installations").

3.5.3.10 Prevention of pollution in case of the hull damage.

¹Hereinafter a nautical mile is equal to 1852 m.

3.5.3.10.1 The ship with the descriptive notations **Oil tanker** or **Oil/ore carrier** or **Chemical tanker** in the class notation shall be provided with double hull and double bottom in the cargo area in accordance with regulation 19 of Annex I to MARPOL 73/78.

3.5.3.10.2 Requirements to the damage trim and stability characteristics specified in 3.3, Part V "Sub-division" shall be used during flooding of any compartment, if provisions of 3.4 of the above Part do not specify more rigid requirements.

3.5.3.10.3 Any ship shall be fitted with the onboard software to calculate intact trim, stability and strength and to calculate damaged ship trim and stability.

3.5.3.10.4 Oil tankers of 600 t deadweight and over, as well as other ships, with an aggregate fuel oil tanks capacity 600 m³ and over shall have prompt access to computerized, shore-based damage stability and residual structural strength calculation programs in accordance with regulation 37.4 of Annex I to MARPOL 73/78.

3.5.3.10.5 Ships having an aggregate fuel oil tanks capacity 600 m³ and over shall have double hull and double bottom to protect fuel oil tanks in accordance with regulation 12A of Annex I to MARPOL 73/78.

3.5.3.10.6 Location of suction wells in fuel oil tanks shall comply with the requirements of regulation 12A.10 of Annex I to MARPOL 73/78.

3.5.3.10.7 The valves for fuel oil pipelines located at a distance less than h from the ship's bottom shall be arranged at a distance of not less than $h/2$ from the ship's bottom (refer to Fig. 3.5.3.10.7).

3.5.3.11 Segregated ballast tanks.

3.5.3.11.1 Segregated ballast tanks shall be provided on ships with the descriptive notation **Oil tanker** or **Oil/ore carrier** or **Chemical tanker** in the class notation.

3.5.3.11.2 The capacity of the segregated ballast tanks shall be so determined that the ship may operate safely on ballast voyages without recourse to the use of cargo tanks for water ballast.

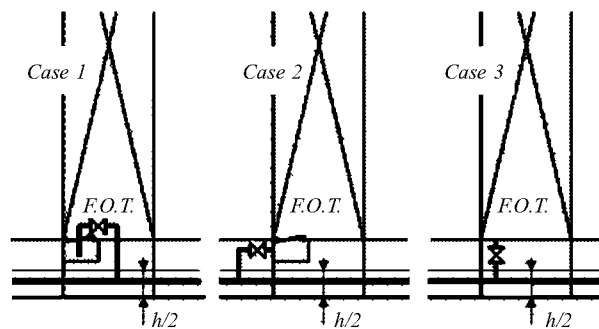
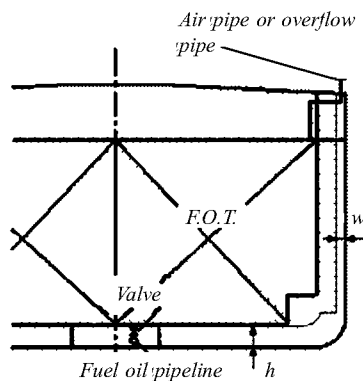


Fig. 3.5.3.10.7

Symbols:

h = the minimum distance of fuel oil tanks location from the moulded line of the bottom shell plating, in m;

w = the minimum distance of fuel oil tanks location from the moulded line of the side shell plating, in m;

F.O.T. = fuel oil tank.

3.5.4 Prevention of pollution at ship recycling.

3.5.4.1 All ships shall have a Statement of Compliance to IMO resolution on Ship Recycling "Green Passport" (form 2.4.8) with Supplement (form 2.4.8-1) according to the Guidelines on Ship Recycling (refer to IMO resolution A.962(23)), with additions or amendments thereto currently adopted.

3.5.4.2 The above Statement with Supplement shall be permanently available on board throughout the ship's operating life. The shipowner shall continuously update the Supplement and include thereto all major ship's structure and equipment changes to maintain the information of the Supplement (form 2.4.8-1) actual.

3.5.5 Environmental responsibilities.

All ships shall have a responsible environmental officer onboard.

This officer shall be responsible for the following:
checking the compliance with the environment pollution prevention requirements;

monitoring the implementation of the relevant procedures;

maintaining the relevant ships' logs;

education and training of personnel in the relevant environmental practices.

The responsible environmental officer may delegate authorities to other crew members remaining responsible for the organization of environment protection measures on board the ship.

3.6 TECHNICAL REQUIREMENTS FOR ASSIGNING THE DISTINGUISHING MARK ECO-S IN THE CLASS NOTATION

3.6.1 Introduction.

3.6.1.1 The provisions of the present Chapter cover the requirements for emissions to air from sources of power, cargo systems of oil tankers and service systems on board the ship, as well as the requirements for discharges to sea from sources of power, shipboard

systems and equipment of machinery spaces, from cargo areas of oil tankers, chemical tankers and NLS tankers, from sewage systems, anti-fouling systems and ballast systems of the ship, as well as the requirements for prevention of pollution by garbage.

3.6.1.2 Requirements for assigning the distinguishing mark **ECO-S** in the class notation are more stringent as regards prevention of air and marine environment pollution as compared to the requirements for assigning the distinguishing mark **ECO** in the class notation.

3.6.1.3 The required documentation is listed in 3.4.3.

3.6.2 Prevention of air pollution.

3.6.2.1 General.

3.6.2.1.1 Compliance with the requirements shall be confirmed in accordance with 3.2 to 3.4.

3.6.2.1.2 Fuel oil to be used onboard shall comply with the requirements of 3.5.2.2.7 to 3.5.2.2.10 and 3.6.2.2.4.

3.6.2.2 Prevention of pollution by emission from marine diesel engines.

3.6.2.2.1 NO_x emission restrictions are applied to engines permanently fitted onboard of power more than 130 kW except engines that are part of any equipment used in emergency solely and engines on lifeboats.

3.6.2.2.2 Level of emission from engines on all ships shall not exceed the following maximum values proceeding from nominal r.p.m. of engines:

13,3 g/Kw h when $n < 130$ r.p.m.;

(44 $n^{(-0,23)} - 0,1$) g/Kw h when $n \geq 130$ r.p.m., but < 2000 r.p.m.;

7,6 g/Kw h when $n \geq 2000$ r.p.m.

3.6.2.2.3 The exhaust gas cleaning system to reduce NO_x emission (if fitted) shall comply with the requirements of 3.5.2.2.

3.6.2.2.4 If a ship operates in SO_x emission control area (including ports) the sulphur content in fuel oil shall not exceed 0,10 per cent. Transition from one type of fuel oil to another while coming in and out of the port or while coming in and out of the SO_x emission control area specified in Annex VI to MARPOL 73/78 shall be registered in the ship's log. When an exhaust gas cleaning system is used, the SO₂ (ppm)/CO₂ (5% v/v) ratio shall not exceed 4.3.

3.6.2.2.5 For engines fitted with the exhaust gas cleaning systems to reduce SO_x emission, the compliance with SO_x emission norms specified in the Guidelines for On-Board Exhaust GAS-SO_x Cleaning System (IMO resolution MEPC.184(59)) shall be confirmed during survey by the Register or other classification society.

3.6.2.3 Prevention of pollution by emission from boilers and inert gas generators.

3.6.2.3.1 Compliance with restrictions of SO_x emission from boilers and inert gas generators is mainly achieved by use of low-sulphur content fuel oil with sulphur content complying with 3.6.2.2.4 to 3.6.2.2.5.

3.6.2.3.2 Alternatively, an exhaust gas cleaning system may be used to reduce SO_x emission to reach

the required level of SO_x emission. The use of such system is subject to special consideration by the Register in each particular case.

3.6.2.4 Prevention of pollution by refrigerant emission.

3.6.2.4.1 The requirements of the present Section for prevention of pollution by refrigerant emission shall comply with the requirements of 3.5.2.4.

3.6.2.4.2 The following substances may be used as refrigerants onboard:

natural refrigerants (such as, ammonia (NH₃) or carbonic acid (CO₂));

hydrofluorocarbon (HFC) with ODP = 0 and GWP < 1890.

3.6.2.4.3 Structural and operational requirements shall comply with 3.5.2.4.4 to 3.5.2.4.8.

3.6.2.5 Prevention of pollution by fire extinguishing media emission.

3.6.2.5.1 Natural fire extinguishing media (such as argon, nitrogen, CO₂) used in fixed fire extinguishing systems are not considered as ozone depleting substances.

3.6.2.5.2 When other fire extinguishing media (for instance, hydrofluorocarbons (HFC) are used in fixed fire extinguishing systems, the media shall have the following properties: GWP < 1650, ODP = 0.

3.6.2.6 Prevention of pollution by volatile organic compounds emission.

In order to prevent emission of VOC from oil tankers carrying crude oil, petroleum products or chemical cargoes with flashpoint < 60 °C, the requirements of 3.5.2.6 shall be applied.

3.6.2.7 Prevention of pollution by emission from shipboard incinerators.

Shipboard incinerator shall comply with the requirements of 3.5.2.7.

3.6.3 Prevention of marine environment pollution.

3.6.3.1 General.

Compliance with the requirements shall be confirmed in accordance with 3.2 to 3.4.

3.6.3.2 Discharge of cargo residues.

3.6.3.2.1 Discharge criteria for cargo residues for tankers carrying crude oil, petroleum products or noxious substances in bulk are specified in 3.5.3.2.

3.6.3.2.2 Each tanker designed for the carriage of noxious substances in bulk shall be equipped with pumps and pipelines, providing stripping of each tank carrying cargoes with pollution categories X, Y and Z, in the way that the quantity of residues in the tank and associated piping does not exceed 50 l in accordance with Annex II to MARPOL 73/78. Discharge of contaminated water to sea shall be carried out by means specified in Annex II to MARPOL 73/78.

3.6.3.2.3 Cargo tanks shall have smooth inner surfaces and be equipped with cargo wells for efficient stripping. Horizontal framing shall be avoided as far as practicable. Corrugated bulkheads may be allowed with the maximum horizontal angle of corrugations of 65°.

3.6.3.2.4 A washing system with the cleaning machines so arranged that all the surfaces of each tank be washed is obligatory.

3.6.3.3 Structural measures and equipment for prevention of oil spills during cargo operations and bunkering.

3.6.3.3.1 Oil tankers, chemical tankers and NLS tankers shall have fitted and implemented means and arrangements to reduce the possibility of oil or NLS spill on deck reaching the sea according to 3.5.3.3.2.

3.6.3.3.2 To collect possible oil spills during cargo operations the main deck in the cargo area shall be fitted with a deck scupper system for collection of the spilled cargo according to 3.5.3.3.3.

3.6.3.3.3 On oil tankers, chemical tankers and NLS tankers all cargo manifolds shall be fitted with spill trays with arrangements for spills collection to the tank according to 3.5.3.3.4.

3.6.3.3.4 In the drainage collecting system, shutoff valves shall be provided to stop the drainage into collecting tanks.

3.6.3.3.5 Oil tankers, chemical tankers and NLS tankers shall be fitted with means to support hoses according to 3.5.3.3.5.

3.6.3.3.6 Oil tankers, chemical tankers and NLS tankers shall be fitted with a closed sounding system with high and maximum level alarms.

3.6.3.3.7 Equipment of tanks for fuel oil, lubricating oil and other petroleum products bunkering in all ships, as well as equipment of bunkering stations, vent and overflow pipes and other areas where petroleum products spills may occur shall comply with the requirements of 3.5.3.3.7 and 3.5.3.3.8.

3.6.3.3.8 Spill trays to collect petroleum products in case of overflow and spillage during bunkering shall be fitted with the closed system for collecting petroleum products to the holding tank or slop tank.

3.6.3.4 Ballast water management.

The requirements of 3.5.3.4 are applicable.

3.6.3.5 Prevention of pollution at oil contaminated water discharge.

3.6.3.5.1 Oil contaminated water discharge requirements apply to all ships according to regulations 15 and 34 of Annex I to MARPOL 73/78.

3.6.3.5.2 The maximum oil content at the outlet of bilge separators fitted onboard shall not exceed 5 ppm.

3.6.3.5.3 The above separators in all cases shall be fitted with 5 ppm bilge alarm and automatic shut-off valve.

3.6.3.5.4 Each ship shall be fitted with the bilge water holding tank of sufficient capacity agreed with the Register for bilge water disposal to reception facilities. Bilge water shall be collected to the above holding tank from all bilge wells of machinery spaces.

3.6.3.6 Prevention of pollution by garbage.

3.6.3.6.1 Prevention of pollution by garbage shall comply with the requirements of 3.5.3.6.

3.6.3.6.2 A ship having the descriptive notation **Passenger ship** in the class notation shall be fitted with the following equipment:

marked containers for garbage of the total capacity to provide 100 per cent discharge of garbage to the shore reception facilities in accordance with the requirements 3.5.3.6;

food wastes comminutors shall provide for comminution to particles not exceeding 25 mm in size;

incinerators shall be type approved according to IMO resolution MEPC.76(40) to provide full solid domestic waste incineration when allowed.

3.6.3.6.3 Ships having the descriptive notation **Passenger ship** in the class notation shall not discharge any waste to sea except for food waste having passed through a comminuter where permitted by international and local legislation.

3.6.3.7 Prevention of pollution by sewage.

3.6.3.7.1 Prevention of pollution by sewage shall be in accordance with 3.5.3.7 and 3.6.3.7.2 to 3.6.3.7.4.

3.6.3.7.2 Ships having the descriptive notation **Passenger ship** in the class notation shall have a sewage holding tank of sufficient capacity to allow storage of both sewage ("black water") and sanitary and domestic waste waters ("grey water") while the ship is in the area where discharge is prohibited. The holding tank shall be fitted with visual and audible alarm operating in case of 80 per cent filling of the tank.

3.6.3.7.3 A ship shall be fitted with the sewage treatment plant being of a type approved according to IMO resolution MEPC.159(55) of the capacity sufficient to process both sewage and sanitary and domestic waste waters simultaneously.

3.6.3.7.4 The sewage treatment plant of ships having the descriptive notation **Passenger ship** in the class notation shall be capable to treat both sewage ("black water") and sanitary and domestic waste waters ("grey water").

3.6.3.8 Control of harmful anti-fouling systems.

The requirements of 3.5.3.8 are applicable.

3.6.3.9 Prevention of lubricating oil and hydraulic oil leakages into seawater.

The requirements of 3.5.3.9 are applicable.

3.6.3.10 Prevention of pollution in case of the hull damage.

3.6.3.10.1 The requirements of 3.5.3.10 are applicable considering the requirements of 3.6.3.10.2.

3.6.3.10.2 Ships having individual fuel oil tank or oil residues tank capacity exceeding 30 m³ shall have double bottom to protect fuel oil tanks and oil residues tanks located in accordance with regulation 12A.6 of Annex I to MARPOL 73/78, even if the aggregate capacity of fuel oil tanks is less than 600 m³.

3.6.3.11 Segregated ballast tanks.

Requirements of 3.5.3.11 are applicable.

3.6.4 Additional technical means.

3.6.4.1 In case of failure of essential machinery of the ship's propulsion plant responsible for maintaining

the ship's manoeuvrability in case of emergency, alternative means shall be provided to keep the ship's manoeuvring characteristics.

The following means may be used as alternative (as far as applicable):

two- and multi-shaft propulsion plants;

stern tube arrangements with the possibility of their repair without ship docking and using environmentally friendly media for lubrication and stern tube bearing cooling;

auxiliary retractable azimuth thrusters to keep the ship's speed and course in case of main propulsion plant damage;

four-blade propellers with detachable blades to ensure propulsion in case of damage to a blade where the opposite blade is removed;

"Power take-in" system to transmit the power from an auxiliary electric power plant to the propeller in case of main engine failure;

thrusters in case of main steering gear damage.

The alternative means to preserve the ship manoeuvrability is subject to special consideration by the Register in each particular case.

3.6.4.2 In addition to the navigational equipment and systems complying with the basic (main applicable) requirements of Part V "Navigational equipment" of the Rules for the Equipment of Sea-Going Ships, a ship shall be fitted with an automatic ground collision avoidance system, and the information on the ship's maneuvering characteristics shall be available on the navigation bridge.

3.6.5 Prevention of pollution at ship recycling.

The requirements of 3.5.4 are applicable.

3.6.6 Environmental responsibilities.

The requirements of 3.5.5 are applicable.

3.7 RECORDS

3.7.1 As a result of applying the requirements of the present Section, the following records will be issued:

.1 Classification Certificate (form 3.1.2) with the distinguishing marks **ECO** or **ECO-S** in the class notation;

.2 Report on Survey of the Ship (form 6.3.10).

4 REQUIREMENTS FOR THE EQUIPMENT OF SHIPS IN COMPLIANCE WITH THE DISTINGUISHING MARK ANTI-ICE IN THE CLASS NOTATION

4.1 GENERAL

4.1.1 Scope of application.

4.1.1.1 The requirements for the equipment of ships in compliance with the distinguishing mark **ANTI-ICE** in the class notation apply to ships the design and equipment of which provide effective icing protection. These requirements are additional to the requirements of Part I "Classification", Part III "Equipment, Arrangements and Outfit", Part VIII "Systems and Piping" and Part XI "Electrical Equipment" of the Rules for the Classification and Construction of Sea-Going Ships, as well as Part II "Life-Saving Appliances", Part III "Signal Means", Part IV "Radio Equipment" and Part V "Navigational Equipment" of the Rules for the Equipment of Sea-Going Ships.

4.1.1.2 Ships complying with the requirements of the present Section may be assigned with the distinguishing mark **ANTI-ICE** added to the character of classification.

4.1.1.3 The distinguishing mark **ANTI-ICE** in the class notation may be assigned to ships under construction and in service.

4.1.2 Definitions and explanations.

For the purpose of the present Section the following definitions and explanations have been adopted.

De-icing is removal of ice appearing on the ship's hull, structures and equipment.

Icing protection is a set of design and organizational measures aimed at reduction of the ship's icing and reduction of labour input into ice removal during operation of the ship.

Icing is a process of ice accretion on the ship's hull, structures and equipment due to sea water splashes or freezing of moisture condensating on the hull from the atmosphere.

Anti-icing is prevention of ice formation on the ship's structures and equipment by means of their heating or relevant covering.

Icing Protection Manual is a document describing actions of the ship's crew to provide icing protection. The scope of the Manual and contents of the information contained therein depend on the ship's type, purpose and area of navigation; they shall be chosen in the most efficient way and agreed with the Register.

4.1.3 Technical documentation.

4.1.3.1 The following technical documentation shall be submitted to the Register for approval to assign the distinguishing mark **ANTI-ICE** in the class notation:

.1 arrangement plan of anti-icing means with indication of their heating capacity;

.2 calculation of heating capacity of anti-icing systems equipment;

- .3 electrical single-line diagram of anti-icing systems with heating cables (if any);
- .4 circuit diagram of steam and/or thermal liquids anti-icing systems (if any);
- .5 arrangement diagram of de-icing means;
- .6 test program for anti-icing systems.

4.1.3.2 The following documents approved by the Register shall be kept onboard:

- .1 Icing Protection Manual;
- .2 Information on Stability including loading cases considering icing.

4.2 TECHNICAL REQUIREMENTS FOR ASSIGNING THE DISTINGUISHING MARK ANTI-ICE IN THE CLASS NOTATION

4.2.1 General.

4.2.1.1 Ships with the distinguishing mark **ANTI-ICE** in the class notation shall as a rule be fitted with a tank of sufficient sheer to provide effective water flow under all operating loading cases.

Assignment of the distinguishing mark **ANTI-ICE** in the class notation to flush deck ships is subject to special consideration by the Register in each particular case.

4.2.1.2 The following anti-icing means may be used:

- .1 heating of structures and equipment by means of steam, thermal liquid or heating cables;
- .2 use of permanent (awnings, casings) or removable (covers) protective covers.

4.2.1.3 Besides heating of structures the following de-icing means may be used:

- .1 washing and firing of ice by means of hot water or steam;
- .2 anti-icing liquids;
- .3 manual mechanical means including pneumatic instrument.

4.2.1.4 The use of alternative de-icing means (inflatable elastic tanks, ultrasonic and impulse means, de-icing coatings etc.) is subject to special consideration by the Register in each particular case.

4.2.1.5 If steam systems are used for anti-icing the requirements of Section 18, Part VIII "Systems and Piping" shall be complied with.

4.2.1.6 If thermal liquid systems are used for anti-icing the requirements of Section 20, Part VIII "Systems and Piping" shall be complied with.

4.2.1.7 If systems with heating cables are used for anti-icing the requirements of 15.4, Part XI "Electrical Equipment" shall be complied with.

4.2.2 Stability and subdivision.

4.2.2.1 Ships with the distinguishing mark **ANTI-ICE** in the class notation shall comply with the requirements of Part IV "Stability" and Part V "Subdivision".

4.2.3 Equipment, arrangements and outfit.

4.2.3.1 Platforms of outer ladders as well as platforms for servicing arrangements and equipment fitted on open decks shall have a grid structure or be equipped with heating elements.

4.2.3.2 Outer ladders located on the escape routes to life-saving appliances as well as muster stations to life-saving appliances (including guard rails) shall be equipped with anti-icing means.

4.2.3.3 Coamings of outer doors leading to the accommodation superstructure spaces and to spaces providing the ship's operation in accordance with its main purpose shall be heated.

Decks in areas of exit from the said spaces shall be equipped with anti-icing means.

4.2.3.4 A passage from the accommodation superstructure spaces to the equipment fitted in the fore part of the ship shall be provided on tankers, including chemical tankers and gas carriers. This passage shall be provided with anti-icing means.

4.2.3.5 Application of anti-icing means to the perched fore structures (masts, foundations of cargo-handling gear, etc.) is subject to special consideration by the Register in each particular case.

4.2.3.6 Side scuttles in the wheelhouse providing the arc of visibility required by 3.2, Part V "Navigational Equipment" of the Rules for the Equipment of Sea-Going Ships according to the ship's class shall be heated.

Windshield wipers on the said side scuttles (if any) shall be heated as well.

4.2.3.7 Shell doors, cargo doors and other closing appliances in the fore part of the ship providing the ship's operation in accordance with its main purpose shall be fitted with means for effective ice removal or other means to provide working capacity of the said appliances in case of icing (for example, with ice-breaking hydraulic cylinders).

4.2.3.8 Design of seals of cargo hatches, shell doors and other closing appliances providing the ship's operation in accordance with its main purpose shall preclude freezing of condensate inside seals.

4.2.3.9 Anti-icing shall be provided for the following arrangements and equipment:

- .1 anchor and mooring equipment including (but not limited to) winches, capstans, windlasses, chain stoppers, drums, control panels;
- .2 arrangements for emergency towing of tankers, including chemical tankers and gas carriers;
- .3 hook releasing devices of lifeboats;
- .4 launching appliances of survival craft (falls on drums, sheaves, winches of launching appliances, winch breaks and other elements engaged in launching);
- .5 liferafts, including hydrostatic releasing devices.

The Register may require taking measures to prevent icing of additional equipment and arrangements in accordance with the ship's main purpose.

4.2.3.10 Lifeboats shall be of enclosed type and be equipped with the relevant heating elements to prevent icing and blocking of access hatches and/or doors.

4.2.3.11 Proper locations shall be provided on board for at-sea storage of removable covers used to prevent icing of equipment and fittings.

4.2.3.12 In addition to the emergency outfit specified in Section 9, Part III "Equipment, Arrangements and Outfit", ships with the distinguishing mark ANTI-ICE in the class notation shall have the necessary de-icing outfit (crowbars, ice-axes, axes, shovels, spades) kept in places of permanent storage and having the relevant marking.

4.2.4 Systems and piping.

4.2.4.1 Sufficient number of scuppers and freeing ports shall be provided for the effective water flow from open decks. Scuppers and freeing ports shall be located so as to preclude water stagnation on decks under all operating loading cases.

4.2.4.2 Ventilation heads of ballast tanks and fresh water tanks shall be fitted with the relevant heating devices.

4.2.4.3 Design of air intakes of main, auxiliary and emergency power plants as well as of ventilation of spaces, which are of great importance for the ship's safety, shall preclude their icing that may cause air duct blockage.

4.2.4.4 Measures shall be taken to preclude freezing of liquid in the pipelines of fire extinguishing systems by means of their effective drying or heating.

Fire hydrants, monitors, fittings and other equipment of fire extinguishing systems fitted on open decks shall be protected from icing by means of heating or removable covers.

Cut-off valve of water and foam fire extinguishing systems shall be fitted in enclosed heated spaces or shall be heated.

4.2.4.5 Hot water or steam supply shall be provided for de-icing on open decks.

4.2.4.6 In addition to 4.2.4.1 to 4.2.4.5 the following items shall be heated on tankers, including chemical tankers and gas carriers:

- .1 ventilation valves and pressure/vacuum valves (P/V valves) of cargo tanks and secondary barriers;
- .2 level, pressure, temperature gauges and gas analysers in cargo tanks located on open decks, if necessary;
- .3 inert gas system elements containing water and located on open decks;
- .4 emergency shut-down system (ESD) on gas carriers.

4.2.4.7 Drives of remotely operated fittings of tankers, including chemical tankers and gas carriers,

fitted on open decks shall be equipped with anti-icing devices.

4.2.4.8 Pipelines equipped with electrical heating shall comply with the requirements of 5.8, Part VIII "Systems and Piping".

4.2.5 Electrical equipment, signal means, radio and navigational equipment.

4.2.5.1 The following electrical equipment, signal means, radio and navigational equipment located on open decks shall be designed so that to prevent icing or shall be heated:

- .1 aerials of radio and navigational equipment (excluding rod aerials), aerial matching devices (if fitted on open decks);
- .2 navigation lights;
- .3 whistles;
- .4 COSPAS-SARSAT satellite emergency position-indicating radio beacons;
- .5 main and emergency lighting of open decks;
- .6 TV cameras used during operation of the ship in accordance with its main purpose;
- .7 aerials of telemetric and dynamic positioning systems.

4.2.5.2 If consumers, which according to 9.3.1, Part XI "Electrical Equipment" shall be fed from the emergency source of electrical power, are fitted with electrical heating, their heating elements shall be also fed from the emergency source of electrical power.

4.3 TESTS

4.3.1 Prior to tests the following shall be submitted to the Register surveyor:

- .1 test program approved by the Register;
- .2 Icing Protection Manual approved by the Register.

4.3.2 Anti-icing systems shall be tested in the scope of the approved program including demonstration of their operation for the purpose specified and measurement of their heating capacity.

4.4 RECORDS

4.4.1 As a result of applying the Requirements for the Equipment of Ships in Compliance with the Distinguishing Mark ANTI-ICE in the Class Notation the following records will be issued:

- .1 Classification Certificate (form 3.1.2) with the distinguishing mark ANTI-ICE in the class notation;
- .2 Report on Survey of the Ship (form 6.3.10).

5 REQUIREMENTS FOR THE EQUIPMENT OF OIL TANKERS FOR CARGO OPERATIONS WITH OFFSHORE TERMINALS

5.1 GENERAL

5.1.1 Scope of application.

5.1.1.1 The requirements for the equipment of oil tankers for cargo operations with offshore terminals are additional to those of Part I "Classification", Part III "Equipment, Arrangements, and Outfit", Part VI "Fire Protection", Part VIII "Systems and Piping", Part IX "Machinery", Part XI "Electrical Equipment" and Part XV "Automation".

5.1.1.2 A distinguishing mark BLS-SPM may be added to the character of classification of ships equipped with the bow loading system and complying with the requirements of the present Section in the full scope.

A distinguishing mark BLS may be added to the character of classification of ships equipped with the bow loading system and complying with the requirements of the present Section except for 5.6.2 to 5.6.9 and 5.6.12 to 5.6.14.

A distinguishing mark SPM may be added to the character of classification of ships which are not equipped with the bow loading system but complying with the requirements in 5.6.2 to 5.6.9 and 5.6.12 to 5.6.14.

5.1.1.3 Distinguishing marks BLS-SPM, BLS and SPM may be assigned to ships under construction and in service.

5.1.2 Definitions.

Single Point Mooring (SPM) is a floating or stationary offshore structure intended for mooring the oil tankers or floating offshore oil-and-gas production units and for offloading at sea or at anchorage.

Offshore terminal is a ship or offshore structure which is used for mooring of the oil tanker for loading the cargo.

Bow loading coupler is a device of special design which is a part of the bow loading system and which is used to connect the cargo hose of the offshore terminal to the ship cargo system.

Bow loading system (BLS) is a set of ship equipment located in the fore end of a ship and intended for loading the cargo to the ship from offshore terminals.

5.1.3 Technical documentation.

5.1.3.1 The following technical documentation (where applicable) shall be submitted to the Register to assign distinguishing marks BLS-SPM, BLS or SPM in the class notation:

.1 BLS general arrangement plan with an indication of the cargo system and mooring equipment including:

bow loading coupler, guide roller, chain stopper, traction winch, hawse storage reel, BLS hull structures, control stations;

.2 description and drawings of the bow loading coupler;

.3 calculation and drawings of hull strengthenings for bow hawses and chain stoppers;

.4 fire protection diagram for BLS area;

.5 diagram and calculation of ventilation of BLS special spaces;

.6 drawings of BLS components and assembly units, which surfaces shall be protected by the materials precluding spark formation;

.7 drawings of electrical equipment layout and cable laying in BLS spaces;

.8 BLS circuit diagrams;

.9 BLS connection circuit diagrams;

.10 diagrams of BLS hydraulic system;

.11 BLS operating manual;

.12 BLS test program.

5.1.3.2 The Register may require additional documents to those listed in 5.1.3.1 proceeding from BLS design features.

5.2 SHIP STRUCTURE

5.2.1 Oil tankers equipped with BLS shall be fitted with CPP and thrusters or active means of ship's steering (AMSS) to enable sufficient maneuverability and ship stabilization during cargo operations.

5.2.2 Ships equipped with the dynamic positioning system shall be fitted with the devices for surveillance, verification, manual correction of the automated thrusters and automated propulsion system.

5.3 SHIP'S SPACES

5.3.1 Spaces where bow loading coupler and disconnecting couplings of the cargo pipeline are located, as well as the areas within the radius of 3 m from them are considered as hazardous zone 1 in accordance with 19.2.3, Part XI "Electrical Equipment".

5.3.2 Spaces adjacent to hazardous spaces and zones shall not open thereto and shall be equipped with the ventilation system providing at least 8 air changes per hour.

5.3.3 A space accommodating the bow loading coupler shall be provided with natural ventilation.

5.4 OPENINGS AND THEIR CLOSING APPLIANCES

5.4.1 Entrances, air inlets and other openings to machinery, service spaces and control stations shall not be faced to bow loading couplers and shall be located at a distance of at least 10 m from them.

5.4.2 Doors closing BLS shall comply with the requirements of 7.4, Part III "Equipment, Arrangements and Outfit".

5.4.3 Doors closing BLS, when in the open position, shall be protected from the contact with the metal parts of the equipment taken from the terminal by hardwood or equivalent electric insulating materials and by materials precluding spark formation.

5.4.4 When securing the BLS door there shall be no friction of spark-forming metals.

5.5 ANCHOR ARRANGEMENT

5.5.1 For the anchor arrangement of oil tankers fitted with BLS, design or procedural measures shall be taken to prevent its operation during loading the cargo through BLS.

5.6 MOORING ARRANGEMENT

5.6.1 Ships intended for operation with single point mooring (SPM) and having distinguishing marks BLS-SPM or SPM in the class notation shall be equipped with the mooring arrangement complying with the requirements of 5.6.2 to 5.6.9, 5.6.12 to 5.6.14.

5.6.2 The choice of the breaking strength of the mooring line shall be confirmed by the calculation and shall be subject to special consideration by the Register in each case.

Mooring lines shall comply with the requirements of 4.2, Part III "Equipment, Arrangements and Outfit".

Two mooring lines shall be used for mooring of ships of 150000 t deadweight and above. Each mooring line shall end with a chafing chain of 8 m in length and 76 mm in diameter.

The chain used for the chafing chain shall meet the requirements of 3.6, Part XIII "Materials" and shall be taken as follows:

Grade 3 for ships having a deadweight of up to 350000 t;

Grade R4 for ships of 350000 t deadweight and above.

5.6.3 The ship shall be equipped with one or two bow chain stoppers for the chain of 76 mm in diameter and one or two bow fairleads of at least 600 mm × 450 mm according to Table 5.6.3.

Table 5.6.3

Ship deadweight, in t	Number of bow chain stoppers	Number of bow fairleads	Safe working load (SWL), in kN
≤100000	1	1	2000
>100000 and <150000	1	1	2500
≥150000	2	2	3500

5.6.4 Bow chain stopper shall be capable of holding the chain of 76 mm in diameter in closed position and shall be designed so that in the open position the said segment of chain and its connection details would freely pass through. The upper yield stress of bow stopper material shall be determined based on the load of at least 2,0 SWL.

5.6.5 Bow chain stoppers shall be located between 2.7 and 3.7 m inboard from the bow fairleads, provided the bow fairlead, stopper and vertical roller (if any) or the winch drum or capstan drum shall be aligned.

5.6.6 In way of the chain stopper location the deck shall be sufficiently strengthened to withstand horizontal loads equal to 2,0 SWL.

5.6.7 The chain stopper shall remain in the closed position when the driving energy disappears. The chain stopper shall be manually driven to be opened.

5.6.8 A single bow fairlead shall be located at the ship centerline. Where two fairleads are fitted they shall be arranged symmetrically on each side of ship's centerline at a distance of 2 to 3 m between them.

The fairlead shall be oval or round in shape, the radius of fairlead rounding shall be at least 3,5 of the chain diameters.

The upper yield stress of fairlead material shall be determined based on the load of at least 2,0 SWL as specified in 5.6.3.

Hull strengthenings in way of the bow fairlead shall be calculated to take up the load equal to 2,0 SWL directed at an angle of $\pm 45^\circ$ in the horizontal plane and $\pm 15^\circ$ in the vertical plane from the fairlead axis.

5.6.9 The arrangement components which are in contact with the chafing chain shall be protected by materials precluding spark formation.

5.6.10 BLS mooring machinery shall comply with the requirements of 1.2, 6.1, 6.4, Part IX "Machinery".

5.6.11 BLS traction winch shall be fitted with a manual drive of drum for release of the hawser when the driving energy disappears.

5.6.12 Where a chain stopper is provided, the braking force of the automatic brake of BLS mooring machinery as required in 6.4.3.1, Part IX "Machinery" may be reduced to the value enabling paying out of the hawser with the constant tension equal to the rated pull of the drive.

5.6.13 The pull at a reel of the mooring winch or capstan used for BLS operation with SPM shall be at least 147 kN.

5.6.14 Where SPM pick-up rope is kept onboard, the winch storage drum used to stow the SPM pick-up rope shall be sufficient size to accommodate the rope of 150 m in length and of 80 mm in diameter.

5.7 SPECIAL ARRANGEMENT

5.7.1 Where a ship with BLS is provided with a special emergency towing arrangement it shall comply with the requirements of 5.6.9 in addition to those specified in 5.7, Part III "Equipment, Arrangements and Outfit".

5.8 SYSTEMS AND PIPING

5.8.1 Cargo system.

5.8.1.1 Cargo piping shall comply with the requirements of 9.2.3 to 9.2.7; 9.3.7, 9.5, Part VIII "Systems and Piping", considering the following:

.1 other facilities to ensure galvanic intrinsic safety may be used instead of those specified in 9.3.7, Part VIII "Systems and Piping" which is subject to special consideration by the Register;

.2 BLS piping shall be self-draining with a drainage to the cargo tank;

.3 provision shall be made for a tray of sufficient capacity with a drainage system for ships having in way of bow loading coupler a spraying system precluding cargo spills propagation.

5.8.1.2 Remote-controlled valves shall comply with the requirements of 4.1.1.2 to 4.1.1.5, Part VIII "Systems and Piping".

5.8.2 Hydraulic systems.

5.8.2.1 Hydraulic systems shall comply with the requirements of 7.3, Part IX "Machinery".

5.8.2.2 Hydraulic accumulators shall be located in the space not communicating with the hazardous spaces as specified in 5.3.1.

5.8.2.3 Hydraulic accumulators shall be provided with devices capable of being manually activated when driving energy disappears.

5.8.2.4 Design of the hydraulic drive of the bow loading coupler and chain stopper shall prevent its opening when driving energy disappears.

5.8.2.5 The possibility of manual disconnection of bow loading coupler from the terminal cargo hose in case of hydraulic system failure shall be provided from the local station.

5.9 SOUNDING ARRANGEMENTS AND AUTOMATION

5.9.1 Cargo control during BLS operation shall be realized from BLS control station that may be located

either in the wheelhouse or in a specially equipped room in the fore part of the ship.

The control station shall be equipped with all necessary monitoring and control instruments to carry out all operations for ship positioning and monitoring of the ship mooring and loading parameters.

Where the BLS control station is located in the fore part of the ship, the requirements of 5.10.2 and 5.12 shall be met.

5.9.2 To provide ship positioning the BLS control station shall be equipped with the following:

.1 control system for the controllable pitch propellers of the main propulsion plant (if any);

.2 thrusters control system;

.3 main engine(s) emergency shutdown arrangement;

.4 steering gear(s) control system;

.5 radar display;

.6 log display;

.7 device for monitoring of dynamic positioning system parameters (if any).

5.9.3 To provide monitoring of ship mooring parameters the BLS control station shall be equipped with the following:

.1 devices for indication and logging by recording device (if any) of hawser and cargo hose tension with actuation of alarm for maximum value;

.2 devices for indication and logging by recording device (if any) of chain tension in chain stopper.

5.9.4 To provide monitoring of ship loading parameters the BLS control station shall be equipped with the following:

.1 device for indication of bow loading coupler position;

.2 device for cargo system valves position indication;

.3 device for cargo tanks level indication and high level alarm;

.4 device for cargo pipe pressure indication at BLS inlet;

.5 device for signal transmission from ship to terminal for cargo pump stop and cargo valve closing on the terminal.

5.9.5 Bow loading coupler, chain stopper, cargo system valves shall be provided with position indicators (open-closed).

5.9.6 BLS control system shall provide blocking of the bow loading coupler inlet valve from being opened until receiving a confirmation that the following actions have been carried out:

.1 terminal cargo hose is properly connected to the bow loading coupler;

.2 sufficient number of ship cargo system valves and BLS cut-off valve are opened, oil tanker is ready for loading the cargo.

5.9.7 BLS control system shall provide blocking of the bow loading coupler inlet valve from being opened in case of BLS mooring arrangement blackout or failure.

5.9.8 Quick-acting emergency shutdown system (ESD) shall be provided for the bow loading coupler. ESD shall provide two operating modes:

.1 first emergency shutdown mode (ESD-1) which shall provide the following:

giving a signal for cargo pump stop on the terminal;

closing the bow loading coupler inlet valve and the terminal discharge valve upon receipt of a signal of emergency pressure drop at ship cargo system inlet;

.2 second emergency shutdown mode (ESD-2) which shall provide the following:

giving a signal for cargo pump stop on the terminal;

closing the terminal discharge valve, the bow loading coupler inlet valve and the BLS cut-off valve upon receipt of a signal of emergency pressure drop at ship cargo system inlet;

disconnection of bow loading coupler;

opening of chain stopper.

ESD-1 and ESD-2 commands shall be given from the BLS control station by means of appropriate controls (buttons, switches). After issuing the command the execution of all the above mentioned functions shall be performed sequentially in automatic mode.

Where ESD-1 mode is deactivated before the above mentioned sequence of operations has been carried out, the operations shall be completed automatically. In this case the bow loading coupler inlet valve and the BLS cut-off valve shall be fully closed.

Where ESD-2 mode is deactivated before the above mentioned sequence of operations has been carried out, the operations shall be immediately interrupted except for the bow loading coupler inlet valve and the BLS cut-off valve which shall be fully closed.

Controls for activation of ESD-1 and ESD-2 modes shall be protected from unauthorized use.

5.9.9 Additionally to automatic system specified in 5.9.7, provision shall be made for back-up manual system of emergency disconnection of bow loading coupler by means of which the independent operations for releasing the chain stopper and the locking arrangement of the bow loading coupler shall be provided.

5.9.10 The sequence and time of cargo operations in the emergency disconnection mode shall ensure minimum cargo leakage and preclude the hydraulic shock in the cargo pipeline.

The time of closing of the bow loading coupler inlet valve and the BLS cut-off valve shall be at least 25 s both in automatic and manual modes. The shorter time of closing shall be proved by the calculation confirming the absence of possibility of hydraulic shock in the cargo pipeline.

5.10 FIRE PROTECTION

5.10.1 Boundaries of spaces where BLS cargo system equipment is located shall comply with the requirements of 2.4, Part VI "Fire Protection".

5.10.2 BLS control station in the fore part of the ship shall comply with the following requirements:

.1 BLS control station shall be of "A-60" class boundaries;

.2 maintenance of surplus pressure shall be provided in the space;

.3 an emergency exit from the space shall be provided.

5.10.3 Fire-fighting equipment and systems shall comply with the requirements of Section 3, Part VI "Fire Protection".

5.10.4 The area where BLS cargo and mooring arrangements are located shall be protected by the foam fire extinguishing system independent from the main system.

5.11 ELECTRICAL EQUIPMENT

5.11.1 Electrical equipment shall comply with the requirements of Part XI "Electrical Equipment".

5.11.2 Electrical equipment fitted in the hazardous areas shall comply with the requirements 2.9, 2.10, 19.2.3 and 19.2.4, Part XI "Electrical Equipment".

5.11.3 Lighting of the loading area and the boundary along it shall provide efficient visual monitoring of the mooring arrangement, cargo hose connection, cargo hose and water surface around.

5.12 COMMUNICATIONS

5.12.1 Where the BLS control station is located in the fore part of the ship, provision shall be made for two-way internal communications between the wheelhouse and the cargo control room in accordance with 3.3.2, Part VII "Machinery Installations" and 7.2, Part XI "Electrical Equipment".

5.12.2 Two-way communications shall be provided between the BLS control station and the terminal.

5.12.3 Emergency communications shall be provided between the BLS control station and the terminal.

5.12.4 Provision shall be made for direct and indirect means enabling to check communications between the BLS control station and the terminal in case of failures and faults during cargo operations.

Whether the surveyor to the Register shall attend the first cargo operations on board the other ships of the series shall be determined proceeding from the BLS tests on board the prototype ship.

5.13 TESTS

5.13.1 All BLS systems and components shall be tested after their installation onboard in accordance with the programs approved by the Register.

5.13.2 The first cargo operation on the prototype ship of the series using BLS shall be carried out in the presence of the surveyor to the Register. At that the BLS operation for the purpose specified shall be checked in accordance with the operating manual.

5.14 RECORDS

5.14.1 The following records are issued on the basis of application of the requirements of the present Section:

.1 Classification Certificate (form 3.1.2) with the distinguishing mark BLS-SPM, BLS or SPM in the class notation;

.2 Report on Survey of the ship (form 6.3.10).

6 REQUIREMENTS FOR THE EQUIPMENT OF SHIPS WITH HELICOPTER FACILITIES

6.1 GENERAL

6.1.1 Application.

6.1.1.1 Requirements for the equipment of ships with helicopter facilities are additional to those of Part I "Classification", Part II "Hull", Part III "Equipment, Arrangements and Outfit", Part IV "Fire Protection", Part VIII "Systems and Piping", Part XI "Electrical Equipment" of the Rules for the Classification and Construction of Sea-Going Ships and Part IV "Radio Equipment" of the Rules for the Equipment of Sea-Going Ships.

6.1.1.2 Ships complying with the requirements of the present Section may be assigned with the following distinguishing marks added to the character of classification:

.1 HELIDECK — for ships fitted with helidecks and complying with the requirements specified in 6.2, 6.3, 6.4.1, 6.6 and 6.7;

.2 HELIDECK-F — for ships fitted with the helicopter refueling facilities and complying with the requirements specified in 6.4.2 (as applicable), 6.5.1 and 6.5.2 (as applicable) in addition to those of 6.1.1.2.1;

.3 HELIDECK-H — for ships fitted with a hangar and complying with the requirements of the present Section in a full scope.

6.1.1.3 Distinguishing marks **HELIDECK**, **HELIDECK-F** or **HELIDECK-H** may be assigned to ships under construction and in service.

6.1.1.4 Ships shall also meet the requirements of International Civil Aviation Organization (ICAO) and the Flag State (if any) for ensuring safe operation of helicopters which shall be confirmed by the relevant statement or certificate issued by the appropriate Civil Aviation Authority.

6.1.2 Definitions.

Hangar is a purpose-built space for helicopter storage, maintenance and repair.

Helicopter is the largest onboard helicopter, for which safe execution of take-off and landing operations is ensured.

Helideck is a purpose-built helicopter landing area including all structures, fire-fighting appliances and other equipment necessary for the safe operation of helicopters.

Helicopter facility is a complex of technical means including a helideck, helicopter refueling facilities and compressed gas or special liquid filling facilities (if any), as well as hangars and spaces where helicopter maintenance facilities are located (if any).

6.1.3 Technical documentation.

6.1.3.1 The following technical documentation shall be submitted to the Register for approval (as applicable)

to assign distinguishing marks **HELIDECK**, **HELIDECK-F** or **HELIDECK-H** in the class notation:

.1 helideck and hangar deck plans with indication of design loads;

.2 scantlings determination of helideck and hangar deck, as well as of deck- and bulkhead stiffeners in way of helicopter tie-down points;

.3 general arrangement plan of a helicopter facility with indication of escape routes, tie-down points, location of life-saving appliances and fire-fighting appliances, arrangement plan and specification of lighting facilities;

.4 drawing of helideck guard rails;

.5 diagram of hydraulic system for the helideck guard rail hoisting and lowering, if any;

.6 diagram of helideck drainage system;

.7 diagram of fuel oil loading, transfer, storage and helicopter refueling system;

.8 diagram of improper aviation fuel collection, storage and defueling system;

.9 diagram of nitrogen system for aviation fuel;

.10 electric diagram of main and emergency lighting in the spaces of helicopter facility arrangement;

.11 circuit diagram of lighting and illumination means for landing area of helideck;

.12 drawings of electrical equipment layout and cable laying on the helideck, in hangar and in other spaces of helicopter facility arrangement;

.13 documentation on the helideck and hangar deck covering;

.14 helicopter facility test program.

6.1.3.2 The Register may require additional documents to those listed in 6.1.3.1 proceeding from the ship design features.

6.2 HELIDECK DESIGN

6.2.1 Helideck arrangement with regard to provision of free horizontal and vertical sectors for helicopter approach, landing and take-off shall comply with the requirements of ICAO and the Flag State (if any).

6.2.2 Helideck arrangement shall provide:

.1 free helicopter approach to helideck from at least three sides;

.2 safety of helicopter take-off and landing operations and maintenance personnel;

.3 helideck location at a maximum possible distance from the ship's hazardous spaces and areas.

6.2.3 Helideck movement area shall generally have a form of a regular or irregular polygon in plan view. The

helideck movement area shall be as large as to contain a circle of diameter not less than the largest dimension of the helicopter with running rotary wing and tail rotor, unless otherwise stipulated by the Flag State rules.

6.2.4 A helideck shall be provided with both main and emergency means of escape and with access for fire-fighting and rescue personnel. These shall be located as far apart from each other as practicable and preferably on the opposite sides of the helideck.

6.2.5 If the helideck forms the ceiling of a deckhouse or superstructure it shall be of "A-60" class.

6.2.6 Helideck shall be made of steel. Aluminum alloys may be used provided the following:

.1 a helideck, irrespective of its type and location, shall be subject to a survey in case of fire on the helideck or in close proximity;

.2 if a helideck is located above the deckhouse or similar structure, the following conditions shall be additionally satisfied:

.2.1 the deckhouse top and bulkheads below the helideck shall have no openings;

.2.2 windows below the helideck shall be provided with steel covers.

6.2.7 Landing and helicopter refueling areas shall be clearly marked and provided with coamings to prevent fuel oil leakage from spreading. The drainage facilities in way of helidecks shall be of steel and shall lead directly overboard independent of any other system and shall be designed so that drainage does not fall on any part of the ship.

6.2.8 The helideck members and supporting structures shall comply with the requirements of 2.12.5.8, Part II "Hull".

6.3 EQUIPMENT OF HELIDECKS

6.3.1 The helideck surface shall be smooth, no steps or recesses are generally allowed on the deck. As an exception, the steps or recesses height shall not exceed 60 mm with the edge slope of 1/3.

6.3.2 Provision shall be made for an antiskid helideck and hangar deck covering ensuring the braking coefficient between the helicopter take-off/landing gear and the deck of at least 0,6 in all weather conditions (notched surface may be applied).

For helicopter operation in winter period the central part of the helideck shall be provided with easily detachable natural fiber net with the area of at least 75 per cent of the helideck area. The net shall be reliably secured to the deck. The dismounted net shall be kept onboard.

6.3.3 Helideck free edges shall be provided with hinged guard rails (safety net) of at least 1,5 m in height, meeting the following requirements:

.1 guard rails shall be reliably secured in a hoist position;

.2 guard rails shall be reliably fixed in a hinged position so as to prevent their hoist due to the effect of airflow from the helicopter rotor;

.3 hinged stanchions shall make an angle of 15° to 20° with the helideck plane providing that the outer contour of the guard rail shall not rise above the helideck coaming;

.4 the net shall be made of a non-combustible material;

.5 guard rail hoisting and lowering shall be performed so as to minimize the risk of personnel falling overboard during the operations;

.6 mesh guard shall withstand a load of 2 kN/m².

6.3.4 To minimize the risk of personnel or equipment sliding from the helideck, the helideck free edges shall have coamings of 50 mm in height. The coamings shall meet the requirements of 6.2.7.

6.3.5 The helideck in way of helicopter parking place and maintenance areas, as well as the hangar (if any) shall be equipped with the relevant tie-down and maintenance facilities (if any). Connection dimensions, arrangement plan and design forces of tie-down facilities shall be agreed upon with the helicopter manufacturer or operator.

6.4 FIRE PROTECTION

6.4.1 Fire protection of helidecks.

6.4.1.1 Helideck shall be protected by a fixed foam fire extinguishing system according to item 20 of Table 3.1.2.1 of Part VI "Fire Protection" with characteristics specified in 3.7.2.12 of Part VI "Fire Protection". The foam concentrate shall be suitable for use with seawater and meet the requirements not interior to those, which are adopted by ICAO. The location and characteristics of the equipment of the foam fire extinguishing system shall provide extinguishing of fire on helicopter high-level units.

6.4.1.2 In close proximity to the helideck the following fire-fighting outfit shall be provided and stored near the means of access to that helideck:

.1 at least two dry powder fire extinguishers having a total capacity not less than 45 kg;

.2 carbon dioxide fire extinguishers having a total capacity not less than 18 kg or equivalent;

.3 at least two nozzles of an approved dual-purpose type with hoses sufficient to reach any part of the helideck;

.4 two sets of fireman's outfits in addition to those required by item 10 of Table 5.1.2, Part VI "Fire Protection";

.5 at least the following equipment stored to provide its immediate use and protection from weather exposure:

adjustable wrench;
 blanket (fire-resistant);
 cutter for bolts with at least 60 cm handle;
 hook, grab or salving;
 hacksaw, heavy duty, complete with 6 spare blades;
 ladder;
 lifeline of 5 mm in diameter and 15 m in length;
 pliers, side-cutting;
 set of assorted screwdrivers;
 harness knife complete with sheath.

6.4.1.3 To provide people rescue from helicopters and liquidation of accident consequences, provision shall be made for life-saving equipment on the helideck in compliance with the requirements of ICAO and the Flag State (if any).

Life-saving equipment shall be stored in adequately painted and tightly-closed containers in close proximity to the helideck. The containers shall be provided with plates specifying the content thereof.

6.4.2 Fire protection of hangars and spaces where helicopter refuelling and maintenance facilities are located.

6.4.2.1 Structural fire protection, fixed fire-extinguishing systems and fire detection and alarm systems and fire-fighting outfit for hangars and spaces where helicopter refueling and maintenance facilities are located shall be similar to those of category A machinery spaces.

6.4.2.2 The boundary structures of hangars and spaces where helicopter refueling and maintenance facilities are located shall be made of steel.

6.4.2.3 "NO SMOKING" signs shall be displayed at appropriate locations in hangars and spaces where helicopter refueling and maintenance facilities are located.

6.4.2.4 Storage of flammable liquids and materials, paint materials, lubricating oils, hydraulic liquids and any types of fuel in hangar is not allowed.

6.5 SYSTEMS AND PIPING

6.5.1 Helicopter refuelling systems.

6.5.1.1 All the equipment used in refueling operations shall be effectively earthed. All the equipment, arrangements, machinery and deck coverings shall be manufactured and installed so as to prevent spark formation.

6.5.1.2 Tanks used for storage of helicopter fuel shall be located on weather deck in specially designed area, which shall be:

.1 as remote as practicable from accommodation and machinery spaces, escape routes and embarkation stations as well as from locations containing sources of ignition;

.2 isolated from areas containing sources of vapour ignition.

6.5.1.3 Tanks used for storage of helicopter fuel and associated equipment shall be protected against mechanical damage and from a fire in an adjacent space or area. Tanks shall be protected against direct sunrays.

6.5.1.4 When equipping tanks for the storage of helicopter fuel with facilities for their emergency jettisoning precautions shall be taken to prevent the tank jettisoned from impact against ship's structures.

6.5.1.5 Where portable storage tanks are used, their construction as well as the mounting and securing arrangements shall be designed considering the tank purpose and possibility of inspections. Electric grounding of the tank shall be provided.

6.5.1.6 The helicopter refueling facilities shall meet the requirements of 13.13, Part VIII "Systems and Piping".

6.5.1.7 Fuel pipelines shall have no stagnant sections. Where it is structurally impossible to avoid stagnant sections, provision shall be made for pipe drainage by means of nitrogen purging or another way of pipeline emptying. The lower parts of piping system shall be provided with drain cocks to remove sediment to improper fuel tank.

Provision to be made for fuel jettisoning from tanks of the helicopter located on the helideck or in hangar to the improper fuel tank.

Provision shall be made for improper fuel delivery to the shore or ship's containers.

6.5.1.8 Helicopter refueling and maintenance facilities shall be provided with an operation manual, including equipment description, a checklist of inspections, requirements for safety measures and equipment maintenance procedures. This manual shall also include the procedures and precautions to be followed during helicopter refueling operations developed in accordance with the recognized safe practices.

6.5.2 Ventilation system of hangars and spaces where helicopter refueling and maintenance facilities are located.

6.5.2.1 The ventilation system of hangars and spaces where helicopter refueling and maintenance facilities are located shall meet the requirements of 12.11, Part VIII "Systems and Piping".

6.6 ELECTRICAL EQUIPMENT

6.6.1 Electrical equipment and electric wiring of hangars and spaces where helicopter refueling and maintenance facilities are located shall comply with the requirements of 2.9, Part XI "Electrical Equipment".

6.6.2 Lighting and illumination means for landing area of helidecks shall comply with the requirements of 6.9, Part XI "Electrical Equipment".

6.7 COMMUNICATIONS

6.7.1 To ensure communication with the helicopter provision shall be made for onboard VHF radiotelephone station. The radio station type and characteristics shall comply with the requirements of ICAO and of the Flag State (if any).

6.7.2 To ensure a three-way communication between the helicopter, the helideck and the wheelhouse, provision shall be made for an adequate number of portable VHF radiotelephone stations with headphones.

6.8 TESTS

6.8.1 All systems and components of the helicopter facility when installed onboard shall be tested according to the programs approved by the Register.

6.8.2 Upon request of the Civil Aviation Authority flight trials may be performed on prototype ships in compliance with the Flag State regulatory documents.

6.9 RECORDS

6.9.1 As a result of applying the requirements of the present Section the following records will be issued:

.1 Classification Certificate (form 3.1.2) with the distinguishing mark **HELIDECK**, **HELIDECK-F** or **HELIDECK-H** in the class notation;

.2 Report on Survey of the Ship (form 6.3.10).

7 REQUIREMENTS FOR SHIP EQUIPMENT TO ENSURE LONG-TERM OPERATION AT LOW TEMPERATURE

7.1 GENERAL

7.1.1 Application.

7.1.1.1 The requirements for ship equipment to ensure long-term operation at low temperature apply to ships intended for operation in cold climatic conditions, including the Gulf of Saint Lawrence, northern part of the Baltic Sea, the Arctic Ocean and Antarctic Seas, and are additional to the requirements of Part I "Classification", Part II "Hull", Part III "Equipment, Arrangements and Outfit", Part VII "Machinery Installations", Part VIII "Systems and Piping", Part IX "Machinery", Part XI "Electrical Equipment" and Part XIII "Materials" of the Rules for the Classification and Construction of Sea-Going Ships, Part II "Life-Saving Appliances", Part III "Signal Means", Part IV "Radio Equipment" and Part V "Navigational Equipment" of the Rules for the Equipment of Sea-Going Ships, as well as the Rules for the Cargo Handling Gear of Sea-Going Ships.

7.1.1.2 For ships complying with the requirements of the present Section a distinguishing mark **WINTERIZATION(DAT)** may be added to the character of classification at the shipowner's request. Design ambient temperature shall be indicated in brackets, for example: **WINTERIZATION(−40)**.

7.1.1.3 The necessary conditions for assigning the distinguishing mark **WINTERIZATION(DAT)** are as follows:

.1 availability of ice category marks not less than **Arc4** in compliance with 2.2.3, Part I "Classification". At shipowner's request the distinguishing mark **WINTERIZATION(DAT)** may be assigned to ships with ice category **Ice3** and below, in this case the extent of compliance with the requirements of the present Section shall be subject to special consideration by the Register;

.2 availability of the distinguishing mark **ANTI-ICE** for ships fitted with equipment for icing protection in compliance with Section 4;

.3 availability of the distinguishing mark for ships of high ecological safety not less than **ECO** in compliance with Section 3.

7.1.1.4 The distinguishing mark **WINTERIZATION(DAT)** may be assigned to ships under construction and in service.

7.1.2 Definitions, explanations and abbreviations.

For the purpose of the present Section the following definitions, explanations and abbreviations have been adopted.

A c c o m m o d a t i o n s p a c e s are spaces complying with the requirements of 1.5.2, Part VI "Fire Protection".

P o l l u t a n t means any substance, which falls within the limits for marine disposal in compliance with MARPOL 73/78.

E n c l o s e d s p a c e is a space with a direct access to the open deck which is fitted with an appropriate closure.

IBC Code — International Code for the Construction and Equipment of Ships Carrying Dangerous Chemicals in Bulk;

L S A C o d e — International Life-Saving Appliances Code;

M A R P O L 7 3 / 7 8 — International Convention for the Prevention of Pollution from Ships, 1973 and Protocol, 1978 thereto.

O p e n s p a c e is a space with a direct access to the open deck which is not fitted with closure or shall be kept open for long periods as regards operational conditions of equipment installed in this space.

D e s i g n a m b i e n t t e m p e r a t u r e (D A T) is the minimum average daily air temperature, in °C, which can take place during a five-year period of ship operation on the routes passing in the most unfavourable waters as regards cooling conditions.

D e s i g n t e m p e r a t u r e o f t h e s t r u c t u r e is the temperature, in °C, assumed for choosing of construction material. When the Rules or this Section contain no additional provisions, the design ambient temperature is assumed as a design temperature of the structure.

T e s t t e m p e r a t u r e is the test temperature of machinery, equipment or materials to confirm their fitness for use at design ambient temperature. Unless otherwise specified in the present Section, the test temperature shall be assumed 10 °C below the design ambient temperature.

W o r k i n g l i q u i d s mean fuel and lubricating materials, and hydraulic oils necessary for normal operation of a ship and its equipment, as well as oil residues.

7.1.3 Technical documentation.

7.1.3.1 The following technical documentation shall be submitted to the Register for approval to assign the distinguishing mark **WINTERIZATION(DAT)** in the class notation:

.1 Manual on operation of ship at low temperature (Winterization Manual);

.2 one line diagrams of electric heating systems (electric heating appliances, systems utilizing heating cables);

.3 certificates for machinery, equipment, arrangements, outfit, foam concentrate, hydraulic liquids and lubricating oils, specified in the present Section, confirming suitability of their use at design ambient temperature;

.4 test programs for the equipment intended for prolonged exposure to low service temperatures, specified in the present Section.

7.1.3.2 The following documents approved by the Register shall be available on board the ship:

.1 Manual on operation of ship at low temperature (Winterization Manual);

.2 Information on Stability including loading cases considering icing;

.3 Information on Damage Trim and Stability;

.4 Ice Ship Safety Certificate (Ice Passport).

7.1.3.3 Technical documentation on products to be submitted for approval in addition to the Rules requirements is specified in the relevant Chapters of the present Section.

7.2 DESIGN TEMPERATURES

7.2.1 Design ambient temperature value is established by the shipowner according to the ship purpose and service conditions.

7.2.2 The following standard values of design ambient temperature are stipulated by the present Section: $-30\text{ }^{\circ}\text{C}$ (the distinguishing mark **WINTERIZATION(-30)**); $-40\text{ }^{\circ}\text{C}$ (the distinguishing mark **WINTERIZATION(-40)**); $-50\text{ }^{\circ}\text{C}$ (the distinguishing mark **WINTERIZATION(-50)**).

7.2.3 Application of the present Section requirements to ships intended for operation at design ambient temperature below $-50\text{ }^{\circ}\text{C}$ is subject to special consideration by the Register.

7.2.4 Design ambient temperature shall not be assumed above the temperature specified in 1.2.3.3 of Part II "Hull" for the appropriate category of ice strengthening without special consideration by the Register.

7.2.5 Design temperature of hull structures shall be assumed according to 1.2.3.4 of Part II "Hull". In this case, design ambient temperature shall be assumed as the value of T_A .

7.2.6 For equipment and machinery installed on the open decks, as well as in the open spaces, the design ambient temperature shall be assumed as design temperature of structures. For equipment and machinery installed in unheated enclosed spaces exposed to the environment and adjoining unheated adjacent enclosed spaces the design ambient temperature shall be assumed as the design temperature. For equipment and machinery installed in unheated enclosed spaces exposed to the environment and adjoining heated adjacent enclosed spaces the temperature of $20\text{ }^{\circ}\text{C}$ above the design ambient temperature shall be assumed as the design temperature of structure.

7.3 GENERAL REQUIREMENTS FOR SHIP DESIGN

7.3.1 Cargo and slop tanks of oil tankers (regardless of deadweight) shall be protected throughout the length

by ballast tanks or compartments not intended for carriage of pollutants in compliance with regulation 19 of Annex I to MARPOL 73/78.

Location of cargo and slop tanks of chemical tankers relative to shell plating shall comply with the requirements of regulation 2.6 of the IBC Code depending on the ship's type. Therewith, for carriage of selected vegetable oils onboard the type 3 chemical tankers the requirements of regulation 4.1.3 of Annex II to MARPOL 73/78 shall be met. Other type 3 chemical tankers, as well as tankers intended for carriage of hazardous substances in bulk shall be fitted with cargo and slop tanks located at least at 760 mm distance from the shell plating.

7.3.2 Ships with an aggregate oil fuel tank capacity of 600 m^3 and above shall have a double-hull construction to protect fuel oil tanks located in compliance with regulation 12A of Annex I to MARPOL 73/78.

Ship having any oil fuel tank with a capacity exceeding 20 m^3 shall have a double-hull construction to protect such tanks located in compliance with paragraphs 6 and 7 of regulation 12A, Annex I to MARPOL 73/78, even in case when the aggregate capacity of fuel oil tanks is below 600 m^3 .

7.3.3 On all ships, the tanks intended for storage of working liquids and carriage of pollutants as a cargo, shall be located at least at 760 mm distance from the shell plating, except the following tanks with individual capacity of 20 m^3 and below located in the double-bottom space of the engine room:

tanks for working liquids;

fuel oil tanks when their total capacity does not exceed 600 m^3 .

7.3.4 Onboard the ships of ice categories **Ice1** — **Arc4** and the ships of polar classes **PC6** and **PC7**, it is allowed to arrange the tanks intended for storage of working liquids in the double-bottom space aft of midships, except fuel oil tanks specified in 7.3.2.

7.3.5 Navigation bridge wings shall be closed.

Angles of view shall meet the requirements of 3.2, Part V "Navigational Equipment" of the Rules for the Equipment of Sea-Going Ships. Bridge front, rear and side windows (including wings) shall be inclined from the vertical plane top out, at an angle of not less 10° and not more than 25° .

7.3.6 Exit from corridors of accommodations to the open deck shall be arranged through the heated companions.

7.3.7 A heated deckhouse shall be provided as a shelter for crew while performing the following functions: observation of the environment during the ship's movement or using guards whilst in a port.

7.3.8 When the ship is equipped for movement in the notch of an icebreaker, the adequate hull strengthening of the fore end shall be provided. Calculations of strengthening shall be submitted to the Register for consideration.

Where necessary, the appropriate arrangements for lifting the anchors from the hawse pipes, as well as the device for their fastening to the deck shall be provided.

7.4 EQUIPMENT, ARRANGEMENTS AND OUTFIT

7.4.1 Anchor arrangement.

7.4.1.1 Materials for manufacture of anchor shall meet the requirements of Section 8, Part XIII "Materials".

7.4.1.2 Materials for manufacture of anchor chain shall meet the requirements of 7.12.7.

7.4.1.3 Materials of castings for manufacture of anchor hawse pipe shall meet the requirements of 7.12.4.

The Register certificates issued for anchor hawse pipes to be installed onboard the ships with distinguishing marks **WINTERIZATION(–40)** and **WINTERIZATION(–50)** shall contain an indication whether it is allowed to use them at appropriate design ambient temperature.

7.4.1.4 Anchor stoppers shall meet the requirements of 3.6.1, Part III "Equipment, Arrangements and Outfit".

The Register certificates issued for anchor stoppers to be installed onboard the ships with distinguishing marks **WINTERIZATION(–40)** and **WINTERIZATION(–50)** shall contain an indication whether it is allowed to use them at appropriate design ambient temperature.

7.4.2 Mooring appliances.

7.4.2.1 Materials of castings for manufacture of mooring bollards, fairleaders and other mooring appliances shall meet the requirements of 7.12.4.

The Register certificates issued for mooring appliances to be installed onboard the ships with distinguishing marks **WINTERIZATION(–40)** and **WINTERIZATION(–50)** shall contain an indication whether it is allowed to use them at appropriate design ambient temperature.

7.4.2.2 Chain stoppers for single-point mooring to offshore terminals shall meet the requirements of 7.4.1.4.

7.4.3 Towing arrangement.

7.4.3.1 Materials of castings for manufacture of bitts, towing bollards, fairleaders, chocks, roller and other towing arrangement shall meet the requirements of 7.12.4.

The Register certificates issued for mooring appliances to be installed onboard the ships with distinguishing marks **WINTERIZATION(–40)** and **WINTERIZATION(–50)** shall contain an indication whether it is allowed to use them at appropriate design ambient temperature.

7.4.3.2 Chains of emergency towing arrangement shall meet the requirements of 7.12.7.

7.4.4 Side scuttles.

7.4.4.1 Side scuttles of wheelhouse and cargo control room shall be provided with heating in compliance with 4.2.3.6 of the present Part.

7.4.4.2 Onboard the ships with distinguishing marks **WINTERIZATION(–40)** and **WINTERIZATION(–50)** the side scuttles with double glass shall be installed in accommodation spaces.

7.4.4.3 When the cargo deck is viewed through the side scuttles of master's cabin, at least one of these side scuttles shall be provided with heating.

7.4.4.4 External access or other equivalent means for cleaning of side scuttles of navigation bridge and cargo control room shall be provided.

7.4.5 Hatchways, shell doors, cargo doors.

7.4.5.1 Materials for manufacture of cargo hatch covers and hatchways of cargo tanks, shell doors, cargo doors, including seals shall meet the requirements of 7.12.1 to 7.12.6.

7.4.5.2 Hydraulic liquids and lubricating oils shall be suitable for use at design ambient temperature.

7.4.5.3 The Register certificates issued for cargo hatch covers and cargo tanks, shell doors, cargo doors to be installed onboard the ships with distinguishing marks **WINTERIZATION(–40)** and **WINTERIZATION(–50)** shall contain an indication whether it is allowed to use them at appropriate design ambient temperature.

7.5 STABILITY AND SUBDIVISION

7.5.1 The requirements of Parts IV "Stability" and V "Subdivision" shall be met.

7.5.2 The ship shall be provided with a reliable draught measurement system whereby the forward and aft draughts can be easily determined.

7.6 MACHINERY INSTALLATIONS

7.6.1 Propulsion plants of ice class ships with distinguishing marks **WINTERIZATION(–30)**, **WINTERIZATION(–40)** and **WINTERIZATION(–50)** shall be capable of maintaining rated power and required rated torque at propeller shafts in a range of rotation speed corresponding to the appropriate operating conditions and modes in accordance with the assigned ice category mark.

7.6.2 Means shall be provided to ensure that machinery may be brought into operation from the dead ship condition without external aid, as well as storage and supply of fuel to the emergency diesel-generator having the following characteristics:

.1 winter diesel fuel with pour point temperature not exceeding -45°C onboard the ships with a distinguishing mark **WINTERIZATION(-40)**;

.2 arctic diesel fuel with pour point temperature not exceeding -55°C onboard the ships with a distinguishing mark **WINTERIZATION(-50)**.

7.6.3 Based on their design, the machinery, shafting, boilers and other pressure vessels, as well as pipelines of systems and fittings, shall remain operative during the ship stay at design ambient temperature.

7.6.4 Onboard the ships with distinguishing marks **WINTERIZATION(-40)** and **WINTERIZATION(-50)** air supply to main engines shall not lead to overcooling of machinery space. Technical means shall be provided to exclude increase of mechanical load on cylinders and pistons and bearings of main engines due to the harmful effect of reduced temperatures of scavenging air.

7.6.5 When environmentally hazardous refrigerants are used, the stern tube seals shall be so designed as to prevent leakage out of the seal housing when operated within the specified modes. Permissible leakage of non-toxic and biologically neutral refrigerants are not considered as pollution from ships.

7.6.6 Technical means shall be provided for complete shaft line turning during the ship stay in close floating ice.

7.6.7 In general, at least two auxiliary boilers shall be provided onboard the ships with distinguishing marks **WINTERIZATION(-40)** and **WINTERIZATION(-50)**.

7.6.8 In general, steel four-bladed propellers with detachable blades shall be used.

7.6.9 Ships shall be provided with technical means for replacing defective blades afloat.

7.7 SYSTEMS AND PIPING

7.7.1 Fittings, formed components, expansion joints.

7.7.1.1 Materials for manufacture of fittings, expansion joints and formed components of pipelines to be installed on the open decks, as well as in the open unheated spaces shall meet the requirements of 7.12.1 to 7.12.6.

7.7.1.2 The Register certificate issued for fittings, expansion joints and formed components of pipelines to be installed onboard the ships with distinguishing marks **WINTERIZATION(-40)** and **WINTERIZATION(-50)** and installed on the open decks, as well as in the open unheated spaces shall contain an indication whether it is allowed to use them at appropriate design ambient temperature.

7.7.1.3 Side fittings installed above the load waterline shall meet the requirements of 4.3.1.2 of "Systems and Piping".

7.7.2 Ballast and sewage systems.

7.7.2.1 Ballast system shall meet the requirements of 8.3.2, Part VIII "Systems and Piping".

7.7.2.2 Discharge pipeline of ballast system shall be provided with heating.

7.7.2.3 Where submerged electrically-driven ballast pumps are used, their serviceability at design ambient temperature shall be ensured and documented; and the relevant information shall be introduced into the certificates issued by the Register.

7.7.2.4 Hydraulic liquids used as working media for ballast pumps driving and remotely controlled fittings shall be suitable for use at design ambient temperature.

7.7.2.5 Sewage holding tanks and pipelines leading thereto shall be located in heated spaces or provided with heating.

7.7.3 Fire extinguishing systems.

7.7.3.1 All fire pumps, including emergency fire pump, shall be placed in spaces with positive temperature.

7.7.3.2 Design of water fire main system and foam fire extinguishing system shall meet the requirements of 3.2 and 3.7, Part VI "Fire Protection" considering the requirements of 4.2.4.4.

7.7.3.3 A foam concentrate for foam fire extinguishing system shall be approved by the Register and be stored in the space with positive temperature.

7.7.3.4 Air-foam nozzles intended for installation onboard the ships with distinguishing marks **WINTERIZATION(-40)** and **WINTERIZATION(-50)** shall work properly at required design ambient temperature and shall have the relevant Register approval.

7.7.3.5 Fire hoses shall meet the requirements of 5.1.4, Part VI "Fire Protection" They shall be approved by the Register and be suitable for operation at design ambient temperature.

7.7.4 Systems of tankers and combination carriers.

7.7.4.1 Cargo system.

7.7.4.1.1 Where submerged electrically-driven ballast pumps are used, their serviceability at design ambient temperature shall be ensured and documented and the relevant information shall be introduced into the certificates issued by the Register.

7.7.4.1.2 Hydraulic liquids used as working media for ballast pumps driving and remotely controlled fittings shall be suitable for use at design ambient temperature.

7.7.4.1.3 The Register certificates issued for cargo hoses of oil and chemical tankers shall contain an indication whether it is allowed to use them at design ambient temperature.

7.7.4.2 Bow loading system.

7.7.4.2.1 Materials of components of the bow loading system shall meet the requirements of 7.12.1 to 7.12.6.

7.7.4.2.2 Hydraulic liquids and lubricating oils shall be suitable for use at design ambient temperature.

7.7.4.2.3 The Register certificates issued for bow loading system to be installed onboard the ships with distinguishing marks **WINTERIZATION(−40)** and **WINTERIZATION(−50)** shall contain an indication whether it is allowed to use it at appropriate design ambient temperature.

7.7.4.3 Inert gas system.

7.7.4.3.1 Sea water supply pipeline for deck water seal shall be provided with heating.

7.7.5 Ventilation system.

7.7.5.1 In addition to the requirements of Section 12, Part VIII "Systems and Piping" the ventilation system shall meet the requirements of **4.2.4.3**.

7.8 DECK MACHINERY

7.8.1 Materials used for manufacture of deck machinery components shall comply with the requirements of 7.12.1 to 7.12.6.

7.8.2 The Register certificates issued for deck machinery intended for installation onboard the ships with distinguishing marks **WINTERIZATION(−40)** and **WINTERIZATION(−50)** shall contain an indication whether it is allowed to use it at appropriate design ambient temperature.

7.8.3 Hydraulic liquids and lubricating oils shall be suitable for use at design ambient temperature.

7.9 LIFE-SAVING APPLIANCES

7.9.1 General requirements for life-saving appliances.

7.9.1.1 Life-saving appliances shall comply with the requirements of Part II "Life-Saving Appliances" of the Rules for the Equipment of Sea-Going Ships; at that, they shall be in the operating condition when stored at design ambient temperature.

7.9.1.2 The Register certificates issued for life-saving appliances intended for ships with distinguishing marks **WINTERIZATION(−40)** and **WINTERIZATION(−50)** shall contain an indication whether it is allowed to use them at appropriate design ambient temperature.

7.9.1.3 Life-saving appliances intended for ships with distinguishing marks **WINTERIZATION(−40)** and **WINTERIZATION(−50)** shall be marked **W(−40)** and **W(−50)** accordingly.

7.9.2 Lifeboats.

7.9.2.1 Lifeboats shall be of an enclosed type and shall comply with the following additional requirements

with regard to Section 6, Part II "Life-Saving Appliances" of the Rules for the Equipment of Sea-Going Ships:

.1 a lifeboat shall provide accommodation for a specified number of persons in warm clothes with personal survival kits stipulated by 7.9.6.2;

.2 a lifeboat keel shall be provided with additional strip of steel or other equivalent material to protect the keel from contact with ice; adequate protection is allowed;

.3 a lifeboat engine shall be equipped with a means for its cold start at design ambient temperature within 2 min from the start; a starter shall be driven from two independent sources of power;

.4 cooling system of a lifeboat engine shall ensure its operation at design ambient temperature;

.5 a lifeboat propeller shall be properly protected from damage by ice;

.6 lifeboat engine fuel oil and oils used shall provide engine safe operation at design ambient temperature;

.7 a lifeboat cockpit shall be electrically heated;

.8 lifeboat scuttles which provide the required visibility from a control station shall be heated;

.9 a lifeboat shall be fitted with a fixed two-way VHF radiotelephone apparatus in compliance with the requirements of 12.2, Part IV "Radio Equipment" of the Rules for the Equipment of Sea-Going Ships; apparatus shall be operable at appropriate design ambient temperature;

.10 drinking water shall be stored in containers that allow for expansion due to freezing;

.11 a lifeboat shall be additionally supplied with a food ration in the quantity equal to 30 per cent of the ration required by the LSA Code to account for high rates of energy expenditure under cold conditions;

.12 a lifeboat on-load release mechanism shall be provided with heating or other measures ensuring safe actuation of a release mechanism at design ambient temperature shall be taken;

.13 a suitable icing removal mallet or another tool for ice accretion removal complying with the requirements of **4.2.3.12** shall be available in the vicinity of a lifeboat.

7.9.3 Rescue boats.

7.9.3.1 Rescue boats shall comply with the following additional requirements with regard to Section 6, Part II "Life-Saving Appliances" of the Rules for the Equipment of Sea-Going Ships:

.1 only rigid rescue boats shall be used;

.2 safe starting of the engine at design ambient temperature shall be provided;

.3 rescue boat engine fuel oil and oils used shall provide engine safe operation at design ambient temperature;

.4 a rescue boat shall be fitted with a fixed two-way VHF radiotelephone apparatus in compliance with the

requirements of 12.2, Part IV "Radio Equipment" of the Rules for the Equipment of Sea-Going Ships; apparatus shall be operable at appropriate design ambient temperature.

7.9.4 Liferrafts.

7.9.4.1 Liferrafts shall comply with the following additional requirements with regard to Section 6, Part II "Life-Saving Appliances" of the Rules for the Equipment of Sea-Going Ships:

.1 inflation of a liferaft shall be completed within 3 min at design ambient temperature;

.2 containers of inflatable liferafts and hydrostatic release units shall be provided with heating or other measures to ensure ease launching, inflation and release of liferafts at design ambient temperature shall be taken;

.3 a manual inflation pump that is proven to be effective at design ambient temperature shall be stored in a heated space in the vicinity of the inflatable liferaft;

.4 liferafts shall be additionally supplied with a food ration in the quantity equal to 30 per cent of the ration required by the LSA Code to account for high rates of energy expenditure under cold conditions;

.5 a suitable icing removal mallet or another tool for ice accretion removal complying with the requirements of 4.2.3.12 shall be available in the vicinity of the liferafts.

7.9.5 Launching appliances of lifeboats, rescue boats and liferafts.

7.9.5.1 Launching appliances of lifeboats, rescue boats and liferafts shall comply with the following additional requirements with regard to Section 6, Part II "Life-Saving Appliances" of the Rules for the Equipment of Sea-Going Ships:

.1 materials used for their manufacture shall comply with the requirements of 7.12.1 to 7.12.6;

.2 hydraulic liquids and lubricating oils used in launching and embarkation appliances shall be suitable for use at design ambient temperature;

.3 electric motors and winches of launching appliances, automatic release hook shall be provided with heating or removable covers; if heating is not provided, a suitable icing removal mallet or another tool for ice accretion removal complying with the requirements of 4.2.3.12 shall be available in the vicinity of the launching appliance;

.4 electric motors, hydraulic drives, winches, brakes and other components of the launching appliance shall be effective at design ambient temperature, their operability shall be confirmed by appropriate testing;

.5 drums with falls, sheaves, winches, winch brakes and other components of the equipment engaged in launching shall be provided with heating or other measures ensuring safe launching of survival craft and rescue boats at design ambient temperature shall be taken.

7.9.6 Group and personal survival kits.

7.9.6.1 In addition to the equipment listed in Section 6, Part II "Life-Saving Appliances" of the Rules for the Equipment of Sea-Going Ships, group and personal survival kits shall be provided.

Personal survival kits (PSK) complying with the requirements of 7.9.6.2 shall be carried onboard the ship with a distinguishing mark **WINTERIZATION(DAT)** in the class notation whenever a voyage is expected to encounter mean daily temperatures below 0 °C.

Group survival kits (GSK) complying with the requirements of 7.9.6.4 shall be carried onboard the ship with a distinguishing mark **WINTERIZATION(DAT)** in the class notation whenever a voyage is expected to encounter ice conditions which may prevent the launching and operation of survival craft.

Sufficient number of group and personal survival kits (as applicable) shall be carried to cover at least 110 per cent of the rated complement of the ship.

7.9.6.2 A personal survival kit shall be stored so that it may be easily retrieved in an emergency situation (in cabins or in dedicated lockers near muster and embarkation stations).

A personal survival kit shall consist of the following items:

.1 clothing:

head protection — 1 (vacuum packed);

neck and face protection — 1 (vacuum packed);

hand protection — mitts — 1 pair (vacuum packed);

hand protection — gloves — 1 pair (vacuum packed), if they are not permanently attached to thermal protective aid;

foot protection — socks — 1 pair (vacuum packed);

foot protection — boots — 1 pair;

personal thermal protective aid complying with the requirements of 6.6, Part II "Life-Saving Appliances" of the Rules for the Equipment of Sea-Going Ships — 1;

approved immersion suit — 1 (not required, if an immersion suit is provided for every person onboard in compliance with 4.2.3.2 of Part II "Life-Saving Appliances" of the Rules for the Equipment of Sea-Going Ships);

thermal underwear — 1 set (vacuum packed);

.2 miscellaneous:

handwarmers for 240 h;

sunglasses — 1;

survival candle — 1;

matches — 2 boxes;

whistle — 1;

drinking mug — 1;

pen knife — 1;

handbook (Arctic Survival) — 1;

carrying bag — 1.

Personal survival kits shall not be opened and used for training purposes and the following notice written in English or the language understood by the crew shall be displayed wherever they are stored:

"CREW MEMBERS AND PASSENGERS ARE REMINDED THAT THEIR PERSONAL SURVIVAL KIT IS FOR EMERGENCY SURVIVAL USE ONLY NEVER REMOVE ITEMS OR SURVIVAL CLOTHING OR TOOLS FROM THE PERSONAL SURVIVAL KIT CARRYING BAG — YOUR LIFE MAY DEPEND ON IT".

7.9.6.3 In addition to the equipment listed in 7.9.6.2, it is recommended to include the following items in a personal survival kit:

- impact-heated thermosoles for boots — 1 pair;
- thermotowels for local body warming — 1 pack;
- disposable diapers — 1 pack.

7.9.6.4 Group survival kit shall be stored in containers so that they may be easily retrieved in emergency; in general, containers shall be located adjacent to survival craft and be stowed on cradles; containers shall be floatable and be designed so that they may be easily moved over the ice.

A group survival kit shall consist of the following items:

.1 group equipment:

- tents — 1 per 6 persons;
- air mattresses — 1 per 2 persons;
- sleeping bags — 1 per 2 persons (vacuum packed);
- stove — 1 per tent;
- stove fuel — 0,5 l per person;
- fuel paste — 2 tubes per stove;
- matches — 2 boxes per tent;
- pan (with sealing lid) — 1 per tent;
- fortified health drink — 5 packets per person;
- flashlight — 1 per tent;
- candles and holders — 5 per tent;
- snow shovel — 1 per tent;
- snow saw — 1 per tent;
- snow knife — 1 per tent;
- tarpaulin — 1 per tent;
- foot protection — Booties — 1 pair per person;
- GSK container — 1;

.2 spare personal equipment (1 set per GSK container):

- head protection — 1 (vacuum packed);
- neck and face protection — 1 (vacuum packed);
- hand protection — mitts — 1 pair (vacuum packed);
- hand protection — gloves — 1 pair (vacuum packed);
- foot protection — socks — 1 pair (vacuum packed);
- foot protection — boots — 1 pair;
- personal thermal aid complying with the requirements of 6.6, Part II "Life-Saving Appliances" of the Rules for the Equipment of Sea-Going Ships — 1;
- thermal underwear — 1 set (vacuum packed);
- handwarmers for 240 h — 1 set;
- sunglasses — 1;
- whistle — 1;
- drinking mug — 1.

7.9.6.5 It is recommended to provide air mattresses included in a group survival kit with a self-inflation system.

7.9.6.6 Where a shot gun or hunting rifle is provided to protect survivors from wildlife, it shall be stored in a secure location readily available in an emergency.

7.10 CARGO GEAR

7.10.1 Cargo handling gear.

7.10.1.1 Materials for manufacture of cargo handling gear elements shall meet the requirements of 3.1 of the Rules for the Cargo Handling Gear of Sea-Going Ships and the requirements of 7.12.1 to 7.12.6.

Design ambient temperature is assumed as design temperature of the structure.

7.10.1.2 When cargo-handling gear is equipped with operator's cabin it shall be provided with heating and fitted with window wiper.

Control panels of the cranes not fitted with cabins, as well as derricks, shall have heating or relevant shelter.

7.10.1.3 Necessary means for cold start of machinery of cargo handling gear at design ambient temperature shall be provided.

7.10.1.4 For hydraulic and electro-hydraulic cargo handling gear, heating of hydraulic liquid shall be provided.

7.10.1.5 Hydraulic liquids and lubricating oils shall be suitable for use at design ambient temperature.

7.10.1.6 The Register certificates issued for cargo handling gear to be installed onboard the ships with distinguishing marks **WINTERIZATION(–40)** and **WINTERIZATION(–50)** shall contain an indication whether it is allowed to use it at appropriate design ambient temperature.

7.10.2 Devices for cargo securing on open decks.

7.10.2.1 Materials of devices for securing cargo on open decks, including guides for fastening of deck containers shall meet the requirements of 7.12.1 to 7.12.4.

7.10.2.2 The Register certificates issued for devices for securing cargo on open decks intended for installation onboard the ships with distinguishing marks **WINTERIZATION(–40)** and **WINTERIZATION(–50)** shall contain an indication whether it is allowed to use them at appropriate design ambient temperature.

7.11 ELECTRICAL, RADIO AND NAVIGATIONAL EQUIPMENT

7.11.1 Installation of cables.

7.11.1.1 Cables to be installed on the open decks and in the open unheated spaces shall be tested at following temperatures:

.1 for ships with distinguishing marks **WINTERIZATION(–30)** and **WINTERIZATION(–40)** at the temperature of $-50\text{ }^{\circ}\text{C}$;

.2 for ships with distinguishing marks **WINTERIZATION(–50)** at the temperature of $-60\text{ }^{\circ}\text{C}$;

.3 when design ambient temperature is below $-50\text{ }^{\circ}\text{C}$ the testing temperature shall be $10\text{ }^{\circ}\text{C}$ lower than the design ambient temperature.

7.11.1.2 Cable intended for installation on open decks shall have indications in the Register Certificate/Type Approval Certificate whether it is allowed to use it at appropriate temperatures.

7.11.1.3 Materials for manufacture of cable fastening parts (hangers, cable boxes, pipes) and cable sealing shall meet the requirements of 7.12.1 to 7.12.4.

7.11.1.4 Means shall be provided to protect cable installed on open decks from mechanical damage at manual ice removal. Cable penetrations through open decks shall be covered by steel enclosures to a height of 0,5 m from the transition point or equipment (whichever is closer).

7.11.2 Equipment.

7.11.2.1 All electric motors, switchboards and control panels provided on the open decks and in the open unheated spaces shall be equipped with the means of anticondensation heating.

7.11.2.2 All electrical equipment intended for installation on the open decks and in the open unheated spaces shall be tested for cold endurance according to 10.5.4.2, Part IV "Technical Supervision During Manufacture of Products" of the Rules for Technical Supervision During Construction of Ships and Manufacture of Materials and Products for Ships at the temperature in the chamber being $10\text{ }^{\circ}\text{C}$ lower than the design ambient temperature or at the temperature of $-40\text{ }^{\circ}\text{C}$ (whichever is lower).

The Register certificates issued for electrical equipment to be installed on the open decks and in the open unheated spaces of ships with a distinguishing mark **WINTERIZATION(–50)** shall contain an indication whether it is allowed to use it at appropriate design ambient temperature.

7.11.2.3 All radio equipment intended for installation on the open decks and in the open unheated spaces shall be tested for cold endurance according to 4.2, Appendix 1 to Section 15, Part IV "Technical Supervision During Manufacture of Products" of the Rules for Technical Supervision During Construction of Ships and Manufacture of Materials and Products for Ships at the working temperature in the chamber equal to design ambient temperature or at the temperature $-40\text{ }^{\circ}\text{C}$ (whichever is lower), and at the limiting temperature in the chamber being $20\text{ }^{\circ}\text{C}$ lower than the design ambient temperature or at the temperature of $-60\text{ }^{\circ}\text{C}$ (whichever is lower).

The Register certificates issued for radio equipment to be installed on the open decks and in the open unheated spaces of ships with a distinguishing mark **WINTERIZATION(–50)** shall contain an indication whether it is allowed to use it at appropriate design ambient temperature.

7.11.2.4 All navigational equipment intended for installation on the open decks and in the open unheated spaces shall be tested for cold endurance according to 4.2, Appendix 1 to Section 16, Part IV "Technical Supervision During Manufacture of Products" of the Rules for Technical Supervision During Construction of Ships and Manufacture of Materials and Products for Ships at the working temperature in the chamber equal to a design ambient temperature or at the temperature of $-40\text{ }^{\circ}\text{C}$ (whichever is lower) and at the maximum permissible temperature in the chamber being $20\text{ }^{\circ}\text{C}$ lower than the design ambient temperature or at the temperature of $-60\text{ }^{\circ}\text{C}$ (whichever is lower).

The Register certificates issued for navigational equipment to be installed on the open decks and in the open unheated spaces of ships with a distinguishing mark **WINTERIZATION(–50)** shall contain an indication whether it is allowed to use it at appropriate design ambient temperature.

7.11.2.5 The list of navigational equipment onboard the ships with a distinguishing mark **WINTERIZATION(DAT)** in the class notation shall meet the requirements of 2.2.3, Part V "Navigational Equipment" of the Rules for the Equipment of Sea-Going Ships in respect of additional requirements for the icebreakers, ships of ice categories **Arc4 – Arc9**, as well as ships of all polar classes.

7.11.3 Lighting and signal means.

7.11.3.1 Ships shall be equipped with at least two suitable searchlights which shall be controllable from conning positions.

7.11.3.2 Searchlights specified in 7.11.3.1 shall be installed to provide, as far as is practicable, all-round illumination suitable for mooring, astern manoeuvres and emergency towing.

7.11.3.3 Searchlights specified in 7.11.3.1 shall be designed so as to prevent icing or shall be provided with heating.

7.11.3.4 Provision shall be made for a manually operated flashing red light visible from astern to indicate when the ship is stopped. This shall be capable of use from any location from which the ship can be maneuvered. The flashing light shall have a range of visibility of at least 2 nautical miles. Construction and characteristics of the light shall meet the applicable requirements of 3.1.6 and 3.2.1, Part III "Signal Means" of the Rules for the Equipment of Sea-Going Ships. Arc of visibility in horizontal and vertical plane shall be the same as for stern lights in compliance with 3.1.2, Part III "Signal Means" of the Rules for the Equipment of Sea-Going Ships.

Searchlights specified in 7.11.3.1 and the light specified in 7.11.3.4 shall be effective at design ambient temperature or at the temperature stated in 3.1.3.3, Part III "Signal Means" of the Rules for the Equipment of Sea-Going Ships (whichever is lower).

7.11.3.5 For double action ships adapted for astern propulsion in ice the additional navigation lights complying with the requirements of Part III "Signal Means" of the Rules for the Equipment of Sea-Going Ships shall be provided.

7.11.4 Electrical heating appliances.

7.11.4.1 Electrical heating fed from emergency sources of electrical power shall be provided for the following ship spaces:

- .1 wheelhouse;
- .2 radioroom (if any);
- .3 main machinery control room;
- .4 cargo control room;
- .5 fire extinguishing station;
- .6 one of public spaces (for instance, messroom);
- .7 hospital;
- .8 engineering workshop.

7.11.4.2 Heating appliances capacity fitted in the above spaces shall provide positive temperature in these spaces at design ambient temperature.

7.11.4.3 Emergency sources of electrical power shall ensure supply of the above heating appliances during the time period stated in 9.3.1, Part XI "Electrical Equipment".

7.11.4.4 Battery compartments shall be heated in compliance with the requirements of 13.3, Part XI "Electrical Equipment". Heating appliances, where fitted, shall be fed from emergency source of electrical power. Thus, it is allowed to perform heating, when power is supplied only from the emergency source of electrical power, by any means in compliance with the international and national standards for explosive atmosphere.

7.12 MATERIALS

7.12.1 Materials used for hull structures and ship machinery items subject to the technical supervision of the Register in accordance with the relevant Parts of the Rules shall comply with the requirements of Part XIII "Materials" and with the Register approved standards and/or with the Register agreed specifications.

7.12.2 Steel plates and sections for hull structural members, ship equipment and machinery intended for prolonged exposure to low service temperatures shall be selected to accordance with 1.2.3, Part II "Hull" with due regard to the adopted value of design ambient temperature. Proceeding from the selected strength level and service conditions, the requirements for steel are specified in 3.2, 3.5, 3.13, 3.14 and 3.17 of Part XIII "Materials".

In particular cases, at the request of the Register, steel for essential hull structures may be used upon receipt of data on crack resistance of the steel. The information received shall be assessed with regard to the requirements of Part XII "Materials" of the Rules for the

Classification, Construction and Equipment of Mobile Offshore Drilling Units and Fixed Offshore Platforms.

7.12.2.1 Steel for machinery and equipment foundations installed on the open decks, in open and enclosed unheated spaces shall comply with the requirements of 1.2.3.1, Part II "Hull" (structural members of category I).

The design temperature of structure shall be assumed according to 7.2.6.

7.12.3 Welded and seamless steel pipes for systems on the open decks and in the open unheated spaces shall comply with the requirements of 3.4 and 3.16, Part XIII "Materials", with the Register approved standards and/or Register agreed specifications.

The material for pipes shall be selected proceeding from the purpose of the systems, with regard to their operating temperature and the requirements of 3.5, Part XIII "Materials" of the Rules, as well as the requirements of Table 2-4, Part IX "Materials and Welding" of the Rules for the Classification and Construction of Gas Carriers for the minimum design temperature of -55°C .

7.12.4 The material of steel forgings and castings for the components of ship equipment, machinery and fittings installed on the open decks and in the open unheated spaces of ships shall comply with the requirements of 3.7 or 3.8, Part XIII "Materials" accordingly, or with the Register approved standards and/or Register agreed specifications.

The material for pipes shall be selected proceeding from the purpose of the forgings and castings, and with regard to their operating temperature and the requirements of 3.5, Part XIII "Materials".

7.12.5 Grey iron and ductile cast iron of ferritic structure is not permitted for the manufacture of components of ship equipment, machinery and fittings installed on the open decks and in the open unheated spaces of ships with a distinguishing mark **WINTERIZATION(DAT)** in the class notation.

7.12.6 Plastics, gasket and seal materials, as well as materials of organic origin used for ship equipment, machinery and fittings and for systems installed on open the decks and in the open unheated spaces of ships shall comply with the applicable requirements of Section 6, Part XIII "Materials", with the Register approved standards and/or with the Register agreed specifications. In addition, a documentary confirmation of the above materials reliability at design temperature shall be submitted.

7.12.6.1 The underwater hull and sides of at least 1,0 m above the upper boundary of the ice strake shall have an ice resistant coating (unless clad steel is used for ice strake plating where the appropriate electrochemical protection is provided). The coating supply documentation shall be agreed between the shipowner, the shipyard and the coating manufacturer and shall be submitted to the Register for consideration.

7.12.6.2 The paint coatings of hull structures, machinery and equipment intended for prolonged exposure to low service temperature shall provide required resistance at the design temperature of the structure. The coating supply documentation shall be agreed between the shipowner, the shipyard and the coating manufacturer and shall be submitted to the Register for consideration.

7.12.7 The use of anchor and mooring chain cables of category 1 is not permitted.

The material for anchor and mooring chain cables shall comply with the requirements of 3.6 and Section 7 of Part XIII "Materials", as well as with the Register approved standards and/or with the Register agreed specifications. The maximum impact test temperature is equal to -20°C .

The results of steel test at operating temperature shall be submitted to the Register.

7.13 TESTS

7.13.1 Generally, the materials and equipment covered by the present Section are tested by the

manufacturer in accordance with the Rules for Technical Supervision during Construction of Ships and Manufacture of Materials and Products for Ships.

7.13.2 After completion of construction of prototype ships with ice strengthening category **Arc4** and above, the additional sea trials in ice conditions shall be feasible due to the program developed by the shipowner and agreed with the Register. During the sea trials of prototype ships in ice conditions, provision may be made for checking the operability of anti-icing systems and equipment intended for exposure to low service temperatures.

7.14 RECORDS

7.14.1 As a result of applying the requirements of the present Section the following records will be issued:

.1 Classification Certificate (form 3.1.2) with the distinguishing mark **WINTERIZATION(DAT)** in the class notation;

.2 Report on Survey of the Ship (form 6.3.10).

Российский морской регистр судоходства
Правила классификации и постройки морских судов
Том 3

Russian Maritime Register of Shipping
Rules for the Classification and Construction of Sea-Going Ships
Volume 3

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**LIST OF CIRCULAR LETTERS AMENDING/SUPPLEMENTING NORMATIVE
DOCUMENT**

(Normative document No. and title)

Item No.	Circular letter No., date of approval	List of amended and supplemented paras

РОССИЙСКИЙ МОРСКОЙ РЕГИСТР СУДОХОДСТВА
ГЛАВНОЕ УПРАВЛЕНИЕ
 Санкт-Петербург



Циркулярное письмо

№ 312-2.1-546_ц от 13.12.2011_г.

КАСАТЕЛЬНО: О новой редакции требований к вертолетным устройствам	Ввод в действие	С 01 января 2012 г.	
	Срок действия до		Срок действия продлен до -
	Отменяет/изменяет/дополняет циркулярное письмо		
ОБЪЕКТ НАБЛЮДЕНИЯ: Суда, ПБУ и МСП в постройке и эксплуатации	№ _____ от _____		
	Количество страниц	1 + 19	
Приложения: Текст изменений и дополнений Правил РС на 19 листах (русский и английский текст)			
Первый заместитель генерального директора - исполнительный директор		Баранов И.А. Ф.И.О.	
Вносит изменения в Правила РС	Название НД и № Правила классификации и постройки морских судов Тома 2 и 3 (НД No. 2-020101-064, 2-020101-064-E)		
<p>Настоящим циркулярным письмом в Правила классификации и постройки морских судов вводится новая редакция раздела 6 части XVII «Дополнительные знаки символа класса и словесные характеристики, определяющие конструктивные или эксплуатационные особенности судна», содержащего требования к вертолетным устройствам.</p> <p>Новая редакция разработана при участии специалистов Государственного Научно-Исследовательского Института Гражданской Авиации с учетом:</p> <ul style="list-style-type: none"> - резолюции ИМО А.1023(26) «Code for the Construction and Equipment of Mobile Offshore Drilling Units, 2009», вступающей в силу с 1 января 2012 г. и содержащей измененные требования к вертолетным устройствам; - требований Международной организации гражданской авиации (ИКАО) с учетом рекомендаций, вступающих в силу с 1 января 2012 г.; - практики применения действующих правил РС. <p>При этом в новую редакцию раздела 6 переносятся требования к вертолетным устройствам, содержащиеся в главах 12.11 и 13.13 части VIII «Системы и трубопроводы» Правил классификации и постройки морских судов и в главе 2.3 части VI «Противопожарная защита» Правил классификации, постройки и оборудования ПБУ и МСП.</p> <p>Текст изменений, который будет внесен при переиздании Правил классификации и постройки морских судов, прилагается.</p>			
<p>Необходимо выполнить следующее:</p> <ol style="list-style-type: none"> 1. Ознакомить инспекторский состав с текстом данного циркулярного письма. 2. Применять новую редакцию требований к судам, ПБУ и МСП, оборудованным вертолетными устройствами, киль которых заложен начиная с 01 января 2012 г. 			
Исполнитель:	Грубов Д.А. Ф.И.О.	007 отд.	(812) 312 24 28 тел.

Правила классификации и постройки морских судов (2012)
(НД № 2-020101-064)

Часть VIII «Системы и трубопроводы»

Текст главы 12.11 заменяется текстом следующего содержания:

12.11 ВЕНТИЛЯЦИЯ АНГАРОВ ДЛЯ ВЕРТОЛЕТОВ

12.11.1 Вентиляция ангаров и помещений для заправки и обслуживания вертолетов, должна отвечать требованиям гл. 6.5 части XVII «Дополнительные знаки символа класса и словесные характеристики, определяющие конструктивные или эксплуатационные характеристики судна».

Текст главы 13.13 заменяется текстом следующего содержания:

13.13 СИСТЕМЫ ЗАПРАВКИ ТОПЛИВОМ ВЕРТОЛЕТОВ

13.13.1 Система топлива, предназначенная для снабжения других судов и вертолетов топливом с температурой вспышки ниже 43 °С, должна отвечать требованиям гл. 6.5 части XVII «Дополнительные знаки символа класса и словесные характеристики, определяющие конструктивные или эксплуатационные особенности судна».

Часть XVII «Дополнительные знаки символа класса и словесные характеристики, определяющие конструктивные или эксплуатационные особенности судна»

Текст раздела 6 «Требования по оборудованию судов вертолетными устройствами» заменяется текстом следующего содержания:

6 ТРЕБОВАНИЯ К ВЕРТОЛЕТНЫМ УСТРОЙСТВАМ

6.1 ОБЩИЕ ПОЛОЖЕНИЯ

6.1.1 Область распространения.

6.1.1.1 Требования к вертолетным устройствам являются дополнительными к требованиям части I «Классификация», части II «Корпус», части III «Устройства, оборудование и снабжение», части VI «Противопожарная защита», части VIII «Системы и трубопроводы», части XI «Электрическое оборудование» Правил классификации и постройки морских судов и части IV «Радиооборудование» Правил по оборудованию морских судов.

6.1.1.2 Судам и морским стационарным платформам (в дальнейшем для данного раздела – судам), отвечающим требованиям настоящего раздела, к основному символу класса могут быть добавлены дополнительные знаки:

.1 HELIDECK – судам, оборудованным вертолетными палубами и удовлетворяющим требованиям 6.2, 6.3, 6.4.1, 6.6 и 6.7;

.2 HELIDECK-F – судам, оборудованным средствами заправки вертолета топливом и удовлетворяющим, в дополнение к 6.1.1.2.1, требованиям 6.4.2 (в зависимости от того, что применимо), 6.5.1 и 6.5.2 (в зависимости от того, что применимо);

.3 HELIDECK-H – судам, оборудованным ангаром и удовлетворяющим требованиям настоящего раздела в полном объеме.

6.1.1.3 Дополнительные знаки **HELIDECK**, **HELIDECK-F** или **HELIDECK-H** могут быть присвоены судам в постройке и судам в эксплуатации.

6.1.1.4 Суда также должны удовлетворять обязательным требованиям Международной организации гражданской авиации (ИКАО) и государства флага (если имеются) по обеспечению безопасной эксплуатации вертолетов, что должно быть подтверждено соответствующим заключением или свидетельством компетентного органа гражданской авиации.

6.1.2 Определения.

Ангар – специальное помещение для хранения и/или технического обслуживания и ремонта вертолетов.

Вертолетная палуба – специально оборудованное на судне место для взлета и посадки вертолетов, включающее всю конструкцию, противопожарные средства и другое оборудование, необходимое для безопасной эксплуатации вертолетов.

Вертолетное устройство (helicopter facility) – комплекс технических средств, включающий вертолетную палубу, устройства для заправки вертолетов топливом и (если имеются) сжатыми газами и специальными жидкостями, а также (если имеются) помещения для обслуживания вертолетов и ангары.

Зона конечного этапа захода на посадку и взлета (final approach and take-off area, FATO) – зона, над которой вертолет завершает маневр захода на посадку, заканчивающийся переходом в режим висения или приземления, или при выполнении маневра взлета начинает поступательный полет.

Зона приземления и отрыва (touchdown and lift-off area, TLOF) – динамически нагруженная площадка, на которой вертолет может выполнить приземление или отрыв. Для вертолетных палуб предполагается, что зоны FATO и TLOF совпадают.

6.1.3 Техническая документация.

6.1.3.1 Для присвоения судну дополнительных знаков **HELIDECK**, **HELIDECK-F** или **HELIDECK-H** в символе класса Регистру должна быть представлена на одобрение следующая техническая документация (в зависимости от того, что применимо):

.1 конструктивные чертежи вертолетной палубы и палубы ангара с указанием величин расчетных нагрузок;

.2 расчеты размеров связей вертолетной палубы и палубы ангара, а также подкреплений палуб и переборок в местах установки средств швартовки вертолета;

.3 чертеж расположения элементов вертолетных устройств с указанием путей эвакуации, мест установки средств швартовки, размещения противопожарного оборудования и спасательных средств, расположения и характеристик светосигнальных и осветительных средств;

.4 чертеж предохранительной сетки;

.5 схема системы силового привода для подъема и заваливания предохранительной сетки, если имеется;

.6 схема системы осушения вертолетной палубы;

- .7 схема системы приема, перекачки, хранения и заправки вертолета топливом;
- .8 схема системы сбора, хранения и выдачи некондиционного авиационного топлива;
- .9 схема системы азота для авиационного топлива;
- .10 схема электрическая основного и аварийного освещения помещений вертолетного устройства,
- .11 схема электрическая светосигнальных и осветительных средств вертолетных устройств;
- .12 чертежи расположения электрического оборудования и прокладки кабелей на вертолетной палубе, в ангаре и в других помещениях вертолетного устройства;
- .13 документация покрытий вертолетной палубы и палубы ангара;
- .14 программа испытаний вертолетного устройства;
- .15 схема ограничения и удаления препятствий, согласованная с уполномоченным органом гражданской авиации государства флага (представляется для сведения);
- .16 схема маркировки вертолетной палубы и препятствий с указанием цвета, размеров и конфигурации знаков, согласованная с уполномоченным органом гражданской авиации государства флага (представляется для сведения).

6.1.3.2 На борту судна должно быть предусмотрено Наставление по эксплуатации средств обслуживания вертолетов (далее - Наставление), включающее описание оборудования, перечень контрольных проверок, требований по мерам безопасности и процедурам обслуживания оборудования. В это Наставление также должны быть включены процедуры и меры предосторожности, которые должны соблюдаться во время операций по заправке вертолетов топливом, разработанные в соответствии с признанной безопасной практикой.

Для плавучих буровых установок (ПБУ) и морских стационарных платформ (МСП) указанное Наставление может быть включено в состав Эксплуатационного руководства, разработанного в соответствии с требованиями гл. 14 Кодекса постройки и оборудования плавучих буровых установок, 2009 г.

6.1.3.3 Исходя из особенностей судна Регистр может потребовать представления дополнительных документов по отношению к указанным в 6.1.3.1.

6.2 КОНСТРУКЦИЯ ВЕРТОЛЕТНЫХ ПАЛУБ

6.2.1 Расположение вертолетной палубы в части обеспечения горизонтальных и вертикальных секторов для подхода, посадки и взлета вертолета должно удовлетворять требованиям ИКАО и государства флага (если имеются).

6.2.2. Размещение вертолетной палубы должно обеспечивать:

- .1 свободные подходы вертолета к вертолетной палубе в соответствии с 6.2.1;
- .2 безопасность выполнения взлетно-посадочных операций и работы технического персонала;
- .3 максимально возможное удаление вертолетной палубы от взрывоопасных помещений и пространств судна.

6.2.3 Вертолетная палуба может иметь в плане любую конфигурацию, как правило, круга или правильного многоугольника. При этом зона FATO должна иметь достаточные размеры, чтобы включать зону, в пределах которой можно поместить круг диаметром не менее наибольшей длины самого большого вертолета с вращающимся несущим и хвостовым винтами (D), для обслуживания которого предназначена вертолетная палуба.

6.2.4 Если вертолетная палуба образует подволоку рубки или надстройки, то она должна быть типа А-60.

6.2.5 Конструкция вертолетной палубы должна быть стальной. Допускается использование алюминиевых сплавов при выполнении следующих условий:

.1 вертолетная палуба независимо от её расположения и типа должна подвергаться освидетельствованию в случае пожара на вертолетной палубе или вблизи неё;

.2 если вертолетная палуба расположена над рубкой или аналогичной конструкцией, она должна дополнительно удовлетворять следующим условиям:

.2.1 верхняя часть рубки и переборки ниже вертолетной палубы не должны иметь отверстий;

.2.2 окна ниже вертолетной палубы должны быть оборудованы стальными крышками.

6.2.6 Для обеспечения осушения вертолетная палуба на МСП должна быть покатой или выпуклой, чтобы избежать скопления дождевых осадков и пролитого топлива на поверхности зоны FATO. Уклоны таких покатых или выпуклых поверхностей должны быть около 1:100. При этом прогиб поверхности вертолетной палубы, вызванный вертолетом в состоянии покоя, не должен приводить к скоплению пролитого топлива на поверхности зоны FATO.

6.2.7 Вертолетные палубы и места заправки вертолетов топливом должны быть четко обозначены и иметь ограждающие комингсы и/или сточные желоба, предотвращающие распространение утечек топлива.

6.2.8 Связи вертолетных палуб и поддерживающие их конструкции должны отвечать требованиям 2.12.5.8 части II «Корпус».

6.3 ОБОРУДОВАНИЕ ВЕРТОЛЕТНЫХ ПАЛУБ

6.3.1 Поверхность вертолетной палубы должна быть ровной, выступы на палубе в зоне FATO, как правило, не допускаются. В виде исключения выступы на границе зоны FATO (с внешней стороны белой линии периметра вертолетной палубы) не должны превышать по высоте 250 мм, а внутри зоны FATO (в границах белой линии периметра вертолетной палубы) не должны превышать по высоте 25 мм. Объекты, которые, исходя из их назначения, должны размещаться на вертолетной палубе внутри зоны FATO, не должны создавать опасности для эксплуатации вертолета.

Для судов, киль которых заложен до 1 января 2012 г., в виде исключения допускаются выступы в зоне FATO высотой не более 60 мм с уклоном кромок 1/3.

6.3.2 Поверхности вертолетной палубы, включая маркировку на ее поверхности, и палубы ангара должны иметь противоскользящее покрытие.

6.3.3 Для эксплуатации вертолета в зимний период в зоне FATO должна устанавливаться легкосъёмная сеть из каната, предпочтительно из натурального волокна (сизаля) диаметром 20 мм с максимальным размером ячеек 200 x 200 мм.

Рекомендуемые размеры сети в зависимости от габаритной длины вертолета определяются достаточностью покрытия посадочного круга:

- 6 м x 6 м при длине вертолета менее 15 м;
- 12 м x 12 м при длине вертолета от 15 до 20 м;
- 15 м x 15 м при длине вертолета более 20 м.

Сеть должна надежно крепиться к палубе по периметру зоны FATO через каждые 1,5 м и быть натянута с усилием не менее 2225 Н.

Снятая сеть должна храниться на судне.

6.3.4 Открытые кромки вертолетной палубы должны быть оборудованы стационарной или заваливающейся предохранительной сеткой шириной не менее 1,5 м, изготовленной из эластичного и негорючего материала.

На плавучих буровых установках и морских стационарных платформах, киль которых заложен до 1 января 2012 г., а также на морских судах, наружная кромка стационарной сетки не должна возвышаться над плоскостью зоны FATO более, чем на 0,25 м, при этом внешний угол наклона сетки вверх должен составлять не менее 10° .

На плавучих буровых установках и морских стационарных платформах, киль которых заложен 1 января 2012 г. и позже, наружная кромка стационарной сетки не должна возвышаться над поверхностью вертолетной палубы, при этом внешний угол наклона сетки должен составлять не менее 10° .

Этим же требованиям должна удовлетворять заваливающаяся сетка в заваленном положении.

Сетка должна без нанесения повреждений выдерживать падение человеческого тела весом 75 кг, при этом сетка не должна действовать как батут.

6.3.5 В дополнение к 6.3.4 заваливающаяся предохранительная сетка должна удовлетворять следующим требованиям:

- .1 сетка должна быть надежно закреплена в поднятом положении;
- .2 сетка должна надежно фиксироваться в заваленном положении от подъема под воздействием воздушного потока от винта вертолета;
- .3 подъем и заваливание сетки должны осуществляться способом, обеспечивающим минимальный риск падения персонала за борт при выполнении операций;
- .4 любой отказ силового привода подъема сетки ограждения не должен препятствовать возможности ее опускания вручную.

6.3.6 Для минимизации риска соскальзывания персонала или оборудования с вертолетных площадок их открытые кромки должны иметь комингсы рекомендуемой высотой 50 мм. Конструкция комингсов должна удовлетворять также 6.2.7.

6.3.7 Вертолетная палуба в местах стоянки и технического обслуживания вертолета, а также ангар (если имеется), должны быть оборудованы средствами для швартовки вертолетов и крепления средств технического обслуживания (если имеются), предпочтительно утопленного типа. Присоединительные размеры, схема расположения и расчетные усилия средств швартовки должны выбираться для раскрепления одного или нескольких типов вертолетов с учетом 6.3.1.

6.3.8 Если входы на вертолетную палубу оборудованы поручнями, высота которых относительно зоны FATO превышает 0,25 м, их конструкция должна обеспечить откидывание, втягивание или удаление при маневрировании вертолета.

6.4 ПРОТИВОПОЖАРНАЯ ЗАЩИТА

6.4.1 Противопожарная защита вертолетных палуб.

6.4.1.1 На вертолетной палубе должны быть предусмотрены как основной, так и аварийный путь эвакуации с нее, а также доступ для персонала пожарной и спасательной партий. Эти пути эвакуации должны располагаться так далеко друг от друга, насколько практически возможно, и предпочтительно - на противоположных сторонах вертолетной палубы.

Если более 50 % площади вертолетной палубы выступает за пределы основной конструкции судна, два входа на вертолетную палубу рекомендуется располагать в пределах таких нависающих участков, что обеспечивает в случае по-

жара на вертолетной палубе наличие по крайней мере одного выхода с нее в наветренную сторону.

6.4.1.2 Вертолетная палуба должна быть защищена стационарной системой пенотушения согласно п. 20 табл. 3.1.2.1 части VI «Противопожарная защита» с характеристиками, указанными в 3.7.2.12 части VI «Противопожарная защита».

Минимальная производительность системы пенотушения вертолетной палубы определяется размером защищаемой площади и расходом пены, при этом минимальная интенсивность подачи раствора должна быть не менее 6 л/м^2 на площадь круга диаметром не менее наибольшей длины вертолета с вращающимися несущим и хвостовым винтами (D).

Количество пенообразователя должно обеспечивать покрытие круга диаметром D в течение не менее 5 мин.

Подача пены при минимальной интенсивности подачи раствора должна начинаться в течение 30 с после включения в действие системы пенотушения.

Пенообразователь должен быть пригоден для использования с морской водой и отвечать требованиям не ниже тех, которые приняты ИКАО.

Размещение и характеристики оборудования системы пенотушения должны обеспечивать тушение высокорасположенных агрегатов вертолета.

Рекомендуется предусматривать дополнительный 100 % запас пенообразователя для обеспечения расчетным количеством пенообразователя на случай приема вертолета после частичного использования запасов пенообразователя при проведении испытаний, учений или тушения пожара.

6.4.1.3 Количество и расположение кранов водопожарной системы должно быть таким, чтобы обеспечить подачу двух струй воды на любую часть вертолетной палубы.

6.4.1.4 В непосредственной близости от вертолетной палубы должно быть предусмотрено и храниться рядом со средствами доступа на эту палубу следующее противопожарное снабжение:

.1 по меньшей мере два порошковых огнетушителя общей вместимостью не менее 45 кг;

.2 углекислотные огнетушители общей вместимостью не менее 18 кг или равноценные им; огнетушители должны быть оборудованы гибкими насадками для тушения возгораний в верхней части вертолета;

.3 по меньшей мере два ствола одобренного комбинированного типа с рукавами достаточной длины для достижения любой части вертолетной палубы;

.4 по меньшей мере два комплекта снаряжения для пожарных, дополнительно к требуемым согласно п. 10 табл. 5.1.2 части VI «Противопожарная защита»;

.5 по меньшей мере следующее оборудование, хранящееся таким образом, чтобы обеспечивалось его незамедлительное использование и защита от воздействия атмосферных условий:

разводной гаечный ключ;

покрывало для тушения пламени;

резак для болтов с рукояткой длиной не менее 60 см;

гак, крюк или пожарный багор;

прочная ножовка по металлу с 6 запасными полотнами;

штормтрап;

спасательный линь диаметром 5 мм и длиной 15 м;

плоскогубцы с боковой режущей кромкой;

набор отверток;

такелажный нож с чехлом;

монтажный лом;

3 пары огнестойких перчаток (рекомендуется);
спасательный топор незаклинивающийся (рекомендуется);
комбинированные ножницы или равнозначный режущий металл инструмент (рекомендуется).

6.4.1.5 Осушительные средства в районе вертолетной палубы должны быть изготовлены из стали или равноценного материала, выводиться непосредственно за борт независимо от любой другой системы и должны быть спроектированы таким образом, чтобы сток не попадал на какую бы то ни было часть судна.

6.4.2 Противопожарная защита помещений для заправки и обслуживания вертолетов и ангаров.

6.4.2.1 Конструктивная противопожарная защита и оборудование стационарными системами пожаротушения и пожарной сигнализации и противопожарным снабжением ангаров и помещений, в которых располагается оборудование для заправки и обслуживания вертолетов, должны быть выполнены как для машинных помещений категории А.

6.4.2.2 Ограничивающие конструкции ангаров и помещений, в которых располагается оборудование для заправки и обслуживания вертолетов, должны быть стальными.

6.4.2.3 Заправочная станция для вертолетов должна удовлетворять следующим требованиям:

.1 ограничивающие конструкции и закрытия отверстий станции должны обеспечивать ее газонепроницаемость. Двери в станцию должны быть стальными;

.2 палуба должна иметь покрытие, исключающее искрообразование, а оборудование, устройства и механизмы должны быть выполнены таким образом, чтобы исключалась возможность искрообразования;

.3 трубопроводы, кабели, проходящие через ограничивающие конструкции станции, не должны нарушать ее газонепроницаемость;

.4 должны быть предусмотрены устройства дистанционной остановки подачи из цистерн топлива из безопасного места в случае возникновения пожара. Если установлена гравитационная система заправки топливом, должно обеспечиваться равноценное устройство отключения подачи топлива;

.5 при наличии нескольких цистерн с топливом схема топливной системы должна предусматривать возможность подачи топлива к заправляемому вертолету одновременно только от одной из них;

.6 слив и сбор пролитого топлива должен производиться в цистерну некондиционного топлива;

.7 трубопроводы топливной системы должны быть изготовлены из стали или равноценного материала, быть по возможности короткими и иметь защиту от повреждений;

.8 установка для заправки вертолетов должна иметь измерительный прибор, регистрирующий количество выданного топлива, гибкий раздаточный шланг со стволом, снабженным самозапорным клапаном, и устройство, исключающее повышение давления в топливной системе сверх допустимого.

6.4.2.4 Количество и расположение кранов водопожарной системы должно быть таким, чтобы обеспечить подачу трех струй воды в любую часть ангара.

6.4.2.5 В ангарах и помещениях, в которых располагается оборудование для заправки и обслуживания вертолетов, в соответствующих местах должны быть надписи «Не курить!».

6.4.2.6 Хранение в ангарах легковоспламеняющихся жидкостей и материалов, лакокрасочных материалов, смазочных масел, гидравлических жидкостей и любых видов топлива не допускается.

6.5 СИСТЕМЫ И ТРУБОПРОВОДЫ

6.5.1 Системы заправки топливом вертолетов.

6.5.1.1 Судовая система заправки топливом вертолетов должна обеспечивать прием, длительное хранение, сохранность качества авиационного топлива и бесперебойное использование в ожидаемых условиях эксплуатации.

6.5.1.2 Все оборудование, используемое при заправочных операциях, должно быть надежно заземлено. Все оборудование, устройства, механизмы и палубные покрытия должны быть выполнены и установлены таким образом, чтобы исключить возможность искрообразования.

6.5.1.3 Цистерны для хранения вертолетного топлива должны располагаться на открытой палубе в специально предназначенном районе, который должен быть:

.1 отдален, насколько это практически возможно, от жилых и машинных помещений, путей эвакуации и мест посадки в спасательные шлюпки, а также мест, имеющих источники воспламенения;

.2 изолирован от мест, содержащих источники воспламенения паров;

.3 в районе хранения топлива должен обеспечиваться сбор пролитого топлива и его слив в цистерну некондиционного топлива;

.4 если цистерны для хранения вертолетного топлива и цистерны некондиционного топлива расположены в закрытых помещениях, то такие цистерны должны быть окружены коффердами, постоянно заполненными инертным газом;

.5 в указанных в 6.5.1.3.4 коффердах длина топливных трубопроводов и число разъёмных трубопроводных соединений должно быть минимальным, а арматура должна располагаться в легко доступном месте, как правило, на открытой палубе;

.6 указанные в 6.5.1.3.4 коффердамы не должны быть связаны с какими-либо трубопроводами, обслуживающими другие помещения.

6.5.1.4 Должен предусматриваться слив топлива из баков вертолета, находящегося на вертолетной палубе или в ангаре, в цистерну некондиционного топлива. Должна предусматриваться выдача некондиционного топлива в береговые или судовые емкости.

6.5.1.5 Цистерны для хранения вертолетного топлива и относящиеся к ним оборудование должны быть защищены от механического повреждения и от пожара в соседнем помещении или районе. Цистерны должны быть защищены от прямого попадания солнечных лучей.

6.5.1.6 При оборудовании цистерн для хранения вертолетного топлива устройствами для их аварийного сброса за борт должны быть приняты меры, предотвращающие удар сбрасываемой цистерны о конструкции судна. Места установки таких цистерн должны располагаться вдали от мест посадки в спасательные шлюпки и плоты и их спуска.

6.5.1.7 Цистерны для хранения вертолетного топлива должны изготавливаться из материалов, стойких к коррозии и воздействию вертолетного топлива.

Топливо может храниться как в съёмных, так и в стационарных цистернах.

Цистерны должны иметь прочное крепление, закрытие и заземление. Цистерны должны быть всегда доступны для осмотра.

Емкости и трубопроводы для противокристаллизационных жидкостей должны изготавливаться из нержавеющей стали.

6.5.1.8 Каждая топливная цистерна должна иметь наполнительную, расходную, измерительную и воздушную трубы. Конец наполнительной трубы должен располагаться не выше 300 мм от днища цистерны. Рекомендуется устанавливать уровнемеры закрытого типа. Измерительная труба должна оканчиваться, не доходя до днища цистерны на 30 — 50 мм, и выводиться на открытую палубу.

6.5.1.9 Воздушные трубы от топливных цистерн должны быть выведены на высоту не менее 2,4 м над открытой палубой. Открытые концы труб должны отстоять на расстоянии не менее 10 м от мест забора воздуха и отверстий, ведущих в закрытые помещения, где находятся источники воспламенения, а также от палубных механизмов и оборудования, которые могут создать опасность воспламенения, и должны быть снабжены пламепрерывающими сетками или другой арматурой, одобренной Регистром.

6.5.1.10 Топливный насос должен одновременно забирать топливо только из одной цистерны. Трубопроводы должны быть изготовлены из стали или равноценного материала, быть по возможности короткими и защищенными от повреждений.

6.5.1.11 Топливные насосы должны иметь средства остановки из удаленного безопасного места. Расходные цистерны должны быть снабжены быстрозапорными клапанами с приводом извне места расположения цистерн.

6.5.1.12 Все трубопроводы и оборудование системы приема, хранения и заправки должны быть электрически непрерывны и надежно заземлены на корпус судна.

6.5.1.13 Трубопроводы системы заправки топливом не должны иметь застойных участков. Если конструктивно невозможно избежать застойных мест, то должна быть предусмотрена возможность осушки трубопроводов путем их продувки азотом или опорожнения другим способом. В нижних точках трубопроводов системы должны быть предусмотрены сливные устройства для удаления отстоя в цистерну некондиционного топлива.

6.5.1.14 Конструкция системы заправки топливом вертолетов должна обеспечивать удобный доступ для выполнения технического осмотра, регламентных работ, отбора проб топлива и ремонта.

6.5.1.15 Судовая система авиационного топлива должна соответствовать требованиям, действующим в гражданской авиации государства флага в части приема, хранения, очистки, контроля качества и выдаче топлива на заправку. Для допуска к эксплуатации топливозаправочное оборудование должно быть сертифицировано (одобрено) на соответствие требованиям авиационных правил государства флага.

6.5.2 Система вентиляции ангаров и помещений для заправки и обслуживания вертолетов.

6.5.2.1 Ангары для вертолетов и помещения, в которых располагается оборудование для заправки и обслуживания вертолетов, должны быть оборудованы искусственной вытяжной вентиляцией кратностью не менее 10 воздухообменов в час. Вентиляторы должны быть взрывозащищенного исполнения и должны отве-

чать требованиям 5.3.3 части IX «Механизмы» и 19.3.4 части XI «Электрическое оборудование».

6.6 ЭЛЕКТРИЧЕСКОЕ ОБОРУДОВАНИЕ

6.6.1. Электрическое оборудование и электрическая проводка в ангарах и помещениях, в которых располагается оборудование для заправки и обслуживания вертолетов, должны отвечать требованиям 2.9 части XI «Электрическое оборудование».

6.6.2 Светосигнальные и осветительные средства вертолетных палуб должны отвечать требованиям 6.9 части XI «Электрическое оборудование» и требованиям гражданской авиации государства флага.

6.7 СРЕДСТВА СВЯЗИ

6.7.1 Для обеспечения полетов судно должно быть оборудовано необходимым радио- и метеорологическим оборудованием в соответствии с требованиями органов гражданской авиации государства флага.

6.8 ИСПЫТАНИЯ

6.8.1 Все системы и компоненты вертолетного устройства после их установки на судне должны быть испытаны в соответствии с одобренными Регистром программами.

6.8.2 На судах по требованию органов гражданской авиации государства флага могут проводиться летные испытания и/или облеты в соответствии с руководящими документами государства флага.

6.9 ОТЧЕТНЫЕ ДОКУМЕНТЫ

6.9.1 По результатам применения Требований выдаются следующие отчетные документы:

.1 Классификационное свидетельство (форма 3.1.2) со знаком **HELIDECK**, **HELIDECK-F** или **HELIDECK-H** в символе класса;

.2 Акт освидетельствования судна (форма 6.3.10).