## CIRCULAR LETTER

No. 313-79-1317c
dated 28.01.2020
Re:
amendments to the Rules for the Classification and Construction of Ships Carrying Liquefied Gases in Bulk, 2020, ND No. 2-020101-131-E

Item(s) of supervision:
pressure relief system
Entry-into-force date:
Valid till:
Validity period extended till:
From the date of publication

Gancels / amends / adds Circular Letter No.
dated
Number of pages: $1+3$
Appendices:
Appendix 1: information on amendments introduced by the Circular Letter
Appendix 2: text of amendments to Part VI "Systems and Piping"
Director General
Konstantin G. Palnikov
Text of CL:
We hereby inform that in connection with coming into force of the IACS Unified Interpretation (UI) GC28
(Rev. 1 Dec 2019) the Rules for the Classification and Construction of Ships Carrying Liquefied Gases in
Bulk shall be amended as specified in the Appendices to the Circular Letter.
It is necessary to do the following:

1. Bring the content of the Circular Letter to the notice of the RS surveyors, as well as interested organizations and persons in the area of the RS Branch Offices' activity.
2. Apply the provisions of the Circular Letter during review and approval of technical documentation on ships, the keels of which are laid or which are at a similar stage of construction on or after 01.01.2020, as well as during review and approval of the technical documentation on ships, the delivery of which is on or after 01.01.2020.

List of the amended and/or introduced paras/chapters/sections:
Part VI: paras 3.16.3 and 3.19.3
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"Thesis" System No. 20-3929

Information on amendments introduced by the Circular Letter (for inclusion in the Revision History to the RS Publication)

| Nos. | Amended <br> paras/chapters/sections | Information on amendments | Number and <br> date of the <br> Circular Letter | Entry-into- <br> force date |
| :--- | :--- | :--- | :--- | :--- |
| 1 | Part VI, para 3.16.3 | Requirements for relieving <br> capacity of pressure relief devices <br> for interbarrier spaces have been <br> specified considering <br> IACS UI GC28 (Rev.1 Dec 2019) | $313-79-1317 \mathrm{c}$ <br> of 28.01.2020 | 28.01 .2020 |
| 2 | Part VI, para 3.19.3 | A new para with the requirements <br> for the calculation of relieving <br> capacity of pressure relief devices <br> for interbarrier spaces has been <br> introduced considering <br> IACS UI GC28 (Rev.1 Dec 2019) | $313-79-1317 \mathrm{c}$ <br> of 28.01.2020 | 28.01 .2020 |

# RULES FOR THE CLASSIFICATION AND CONSTRUCTION OF SHIPS CARRYING LIQUEFIED GASES IN BULK, 2020 

## ND No 2-020101-131-E

## PART VI. SYSTEM AND PIPING

## 3 CARGO SYSTEM

$1 \quad$ Para 3.16.3 is replaced by the following text:
"3.16.3 Interbarrier spaces shall be provided with pressure relief devices approved by the Register.

The required relieving capacity of pressure relief devices of interbarrier spaces surrounding cargo tanks of various designs shall be determined as follows:
.1 the relieving capacity of pressure relief devices of interbarrier spaces surrounding independent type A cargo tanks shall be determined in accordance with 3.19.3;
.2 the relieving capacity of pressure relief devices of interbarrier spaces surrounding independent type B cargo tanks may be determined in accordance with 3.19.3, however, the leakage rate shall be determined in accordance with 7.2, Part IV "Cargo Containment";
.3 the relieving capacity of pressure relief devices for interbarrier spaces of membrane and semi-membrane tanks shall be evaluated on the basis of specific membrane/semi-membrane tank design;
.4 the relieving capacity of pressure relief devices for interbarrier spaces adjacent to integral tanks may, if applicable, be determined in accordance with 3.19.3.".

## 2 A new para 3.19.3 is introduced reading as follows:

"3.19.3 The combined relieving capacity of the pressure relief devices for interbarrier spaces surrounding type A independent cargo tanks is determined by the following formula:

$$
\begin{equation*}
Q_{s a}=3,4 A_{c} \frac{\rho}{\rho_{v}} \sqrt{h} \tag{3.19.3}
\end{equation*}
$$

where $\quad Q_{s a}=$ minimum required discharge rate of air, in $\mathrm{m}^{3} / \mathrm{s}$, at standard conditions ( $0^{\circ} \mathrm{C}$ and $0,1013 \mathrm{MPa}$ );
$A_{c}=$ design crack opening area, in $\mathrm{m}^{2}$;
$A_{c}=\frac{\pi}{4} \delta * L$;
$\delta=\max$, crack opening width, $m$;
$\delta=0,2 t ;$
$t=$ thickness of tank bottom plating, in m ;
$L=$ design crack length, in $m$, equal to the diagonal of the largest plate panel of the tank bottom, as shown in Fig. 3.19.3;
$h=$ max liquid height above tank bottom plus 100•MARVS, in m;
$\rho=$ density of product liquid phase, in $\mathrm{kg} / \mathrm{m}^{3}$, at the set pressure of the interbarrier space relief device;
$\rho_{v}=$ density of product vapour phase, in $\mathrm{kg} / \mathrm{m}^{3}$, at the set pressure of the interbarrier space relief device and a temperature of $0^{\circ} \mathrm{C}$;
MARVS = max allowable relief valve setting of the cargo tank, MPa.


Fig. 3.19.3

